

# Development of intelligent systems (RInS)

## Robot manipulation

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Literature: Tadej Bajd (2006) Osnove robotike, poglavje 4  
Anže Rezelj (2017) Razvoj nizkocenovnega  
lahkega robotskega manipulatorja

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# Robot manipulator

- Industrial robot as defined by the standard ISO 8373:

An automatically controlled, reprogrammable, multipurpose manipulator programmable in three or more axes, which can be either fixed in place or mobile for use in industrial automation applications.



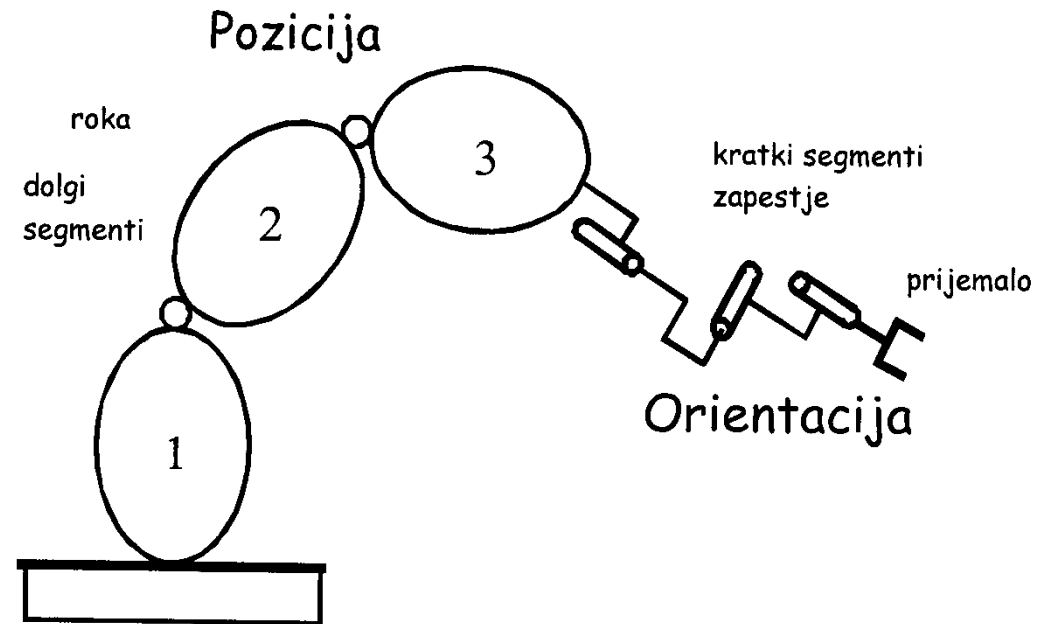
# Characteristics

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- Closed-loop control
  - Electrical or hydraulic motors
  - Sensors
    - Proprioceptive: rotation encoders, measurement of distance, speed
    - Exteroceptive: tactile sensors, robot vision
- Reprogrammable:
  - designed so that the programmed motions or auxiliary functions can be changed without physical alteration
- Multipurpose:
  - capable of being adapted to a different application with physical alteration
- Physical alteration:
  - alteration of the mechanical system
  - fixed or mobile robots
- Axis: direction used to specify the robot motion in a linear or rotary mode
  - 3 or more DOF

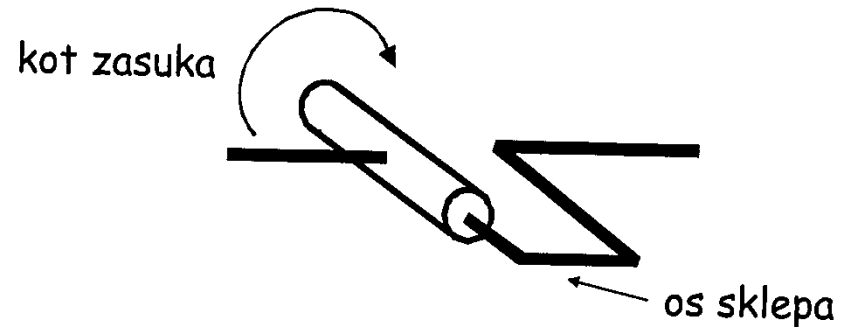
# Robot manipulator

- Arm+wrist+end effector/gripper
- 6DOF – can put an object in an arbitrary pose
  - arm positions the object into the desired position
  - wrist rotates it into the desired orientation
  - gripper grasps the object

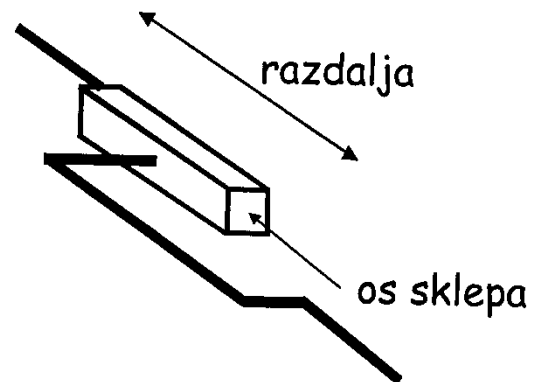


# Robot arm

- Serial chain of three links
- connected by joints
- Revolute/rotational joint



- Prismatic/translational joint



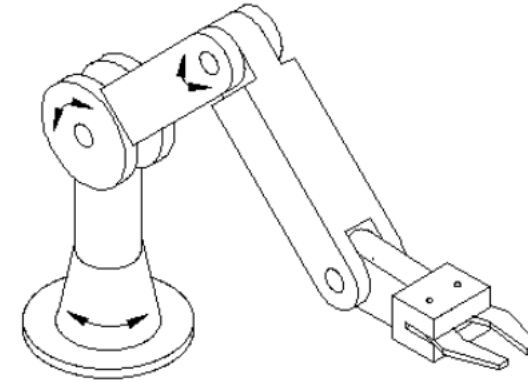
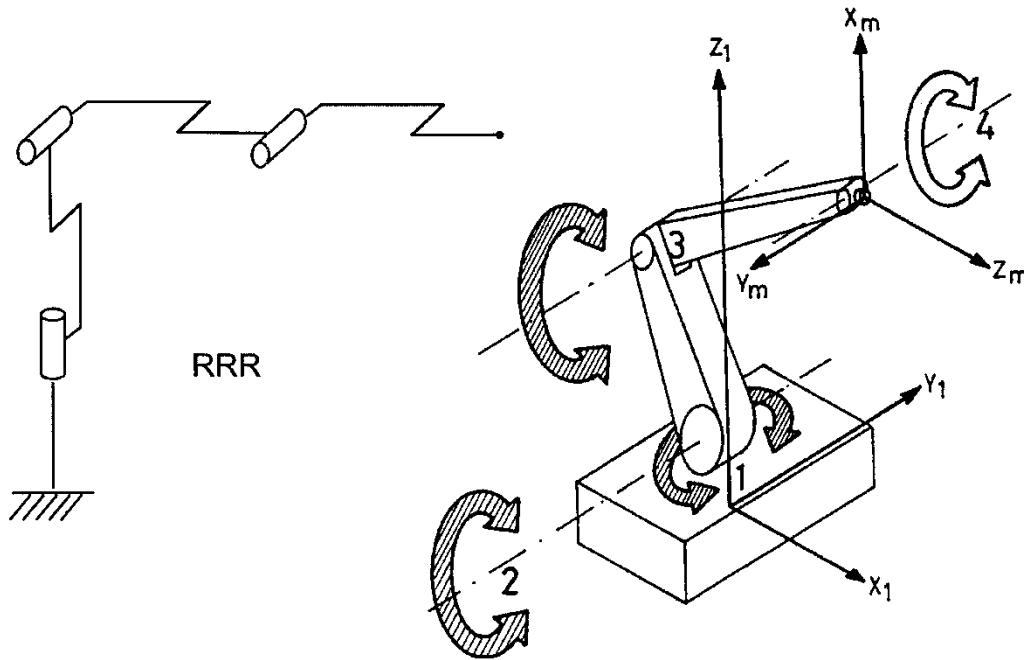
# Robot arm types

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- Joints
  - Revolute/rotational
  - Prismatic/translational
- Axis of two neighbouring links
  - Parallel
  - Perpendicular
- 3DOF
- In practice typically five different arms:
  - Anthropomorphic
  - Spherical
  - SCARA
  - Cylindrical
  - Cartesian

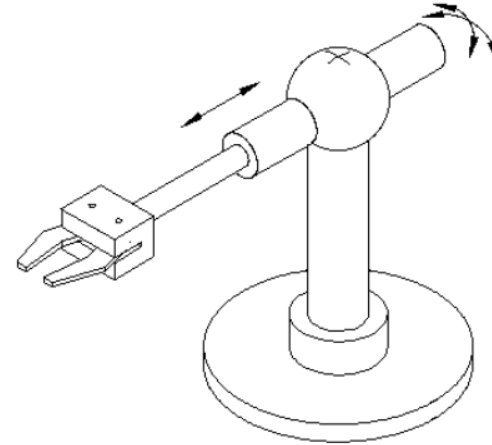
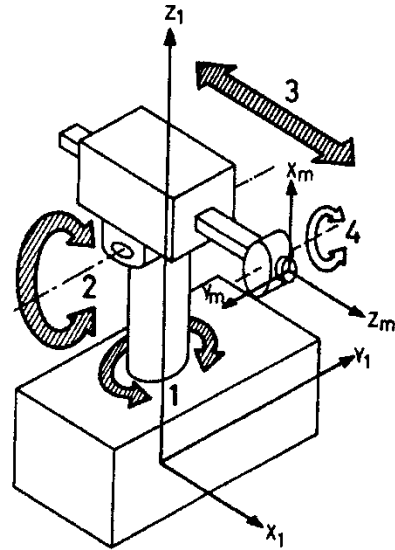
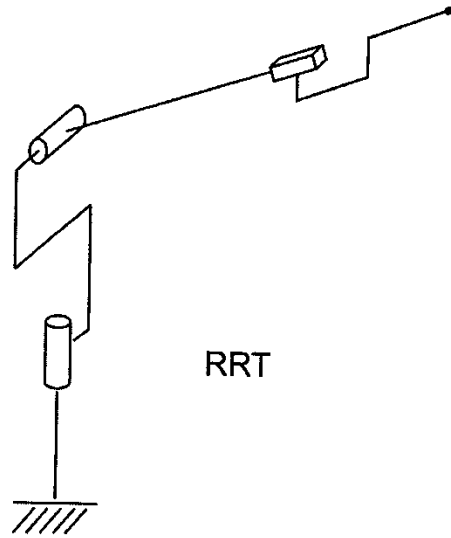
# Anthropomorphic robot arm

- Three rotational joints (RRR)
- Workspace: sphere-like
- Resembles a human arm



# Spherical robot arm

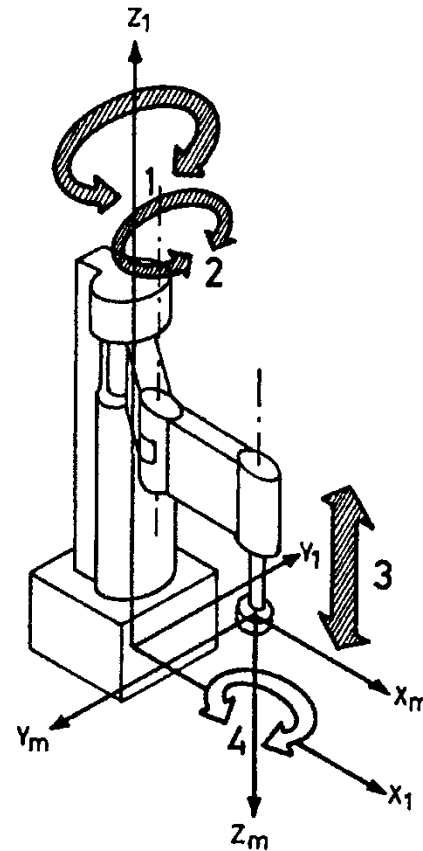
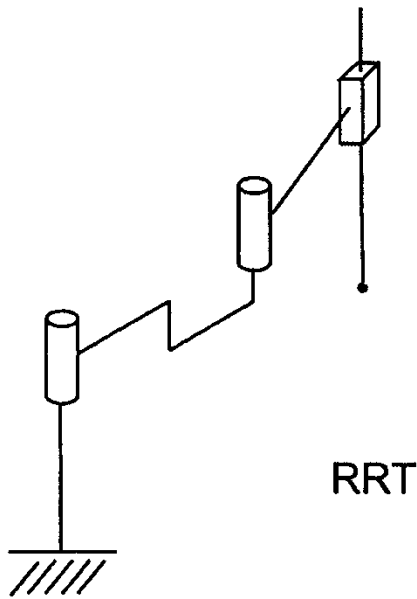
- Two rotational, one translational joint (RRT)
- Workspace: sphere-like





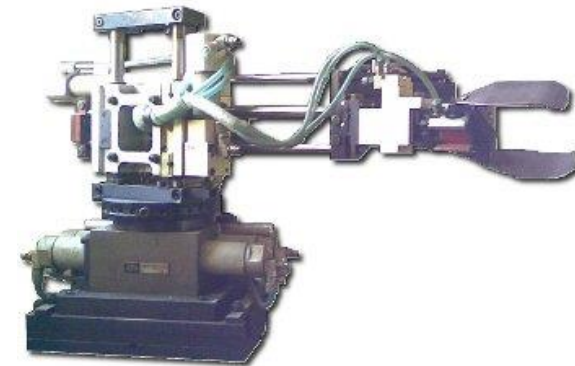
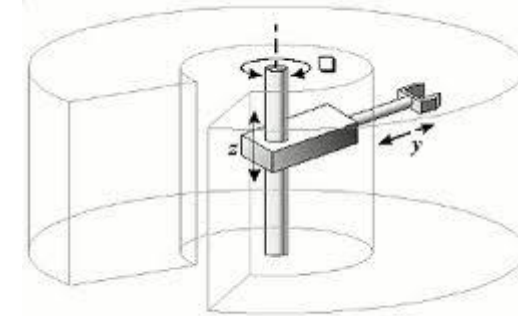
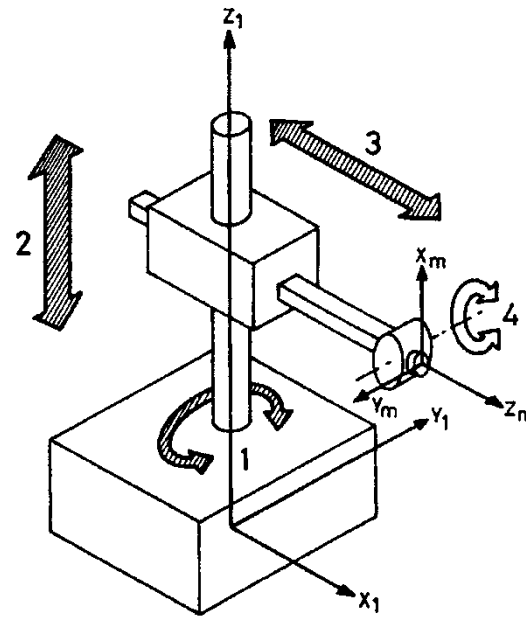
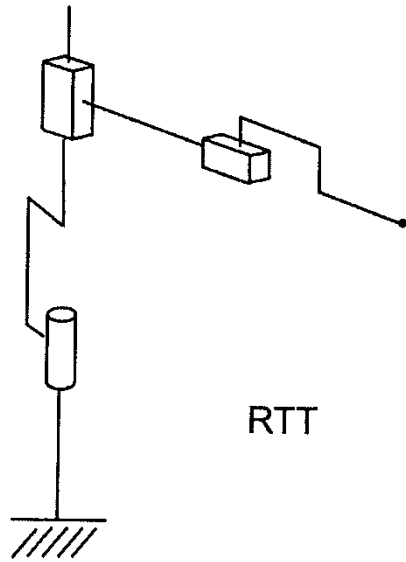
# SCARA robot arm

- Selective Articulated Robot for Assembly
- Two rotational, one translational joint (RRT)
- Workspace: cylinder-like



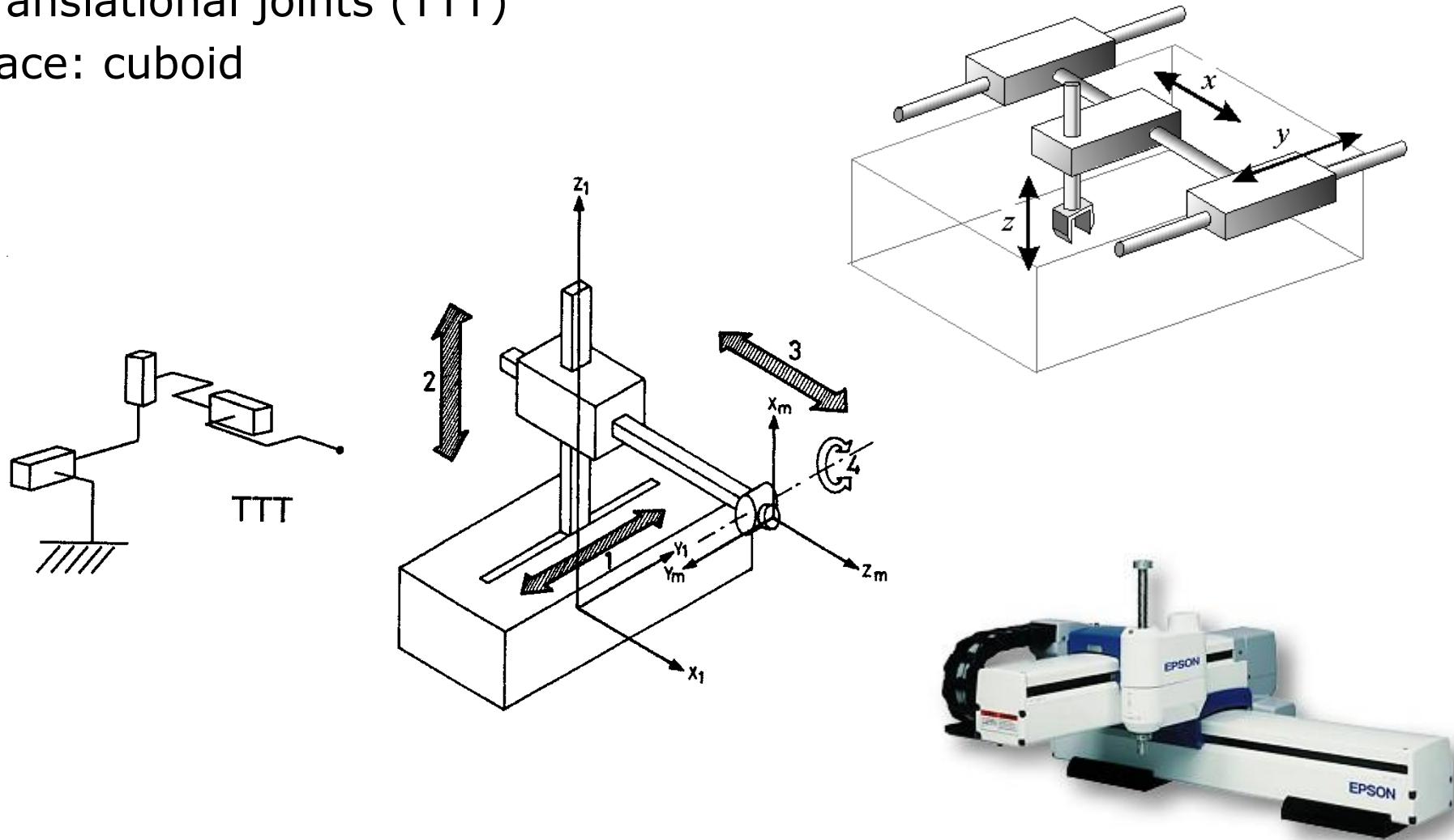
# Cylindrical robot arm

- One rotational, two translational joints (RTT)
- Workspace: cylinder



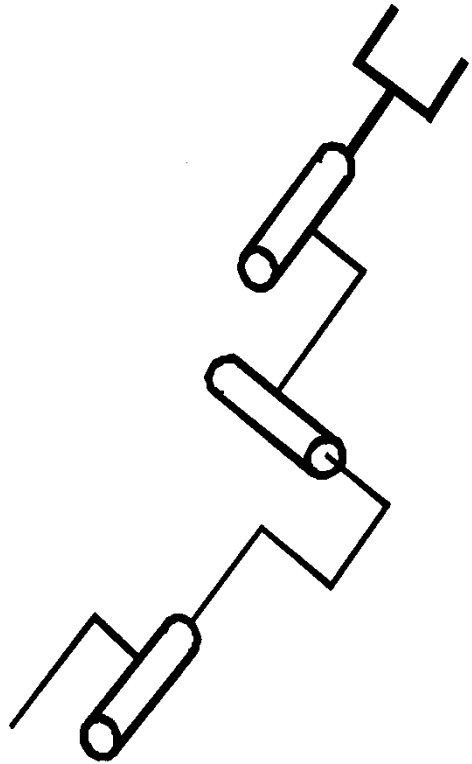
# Cartesian robot arm

- Three translational joints (TTT)
- Workspace: cuboid



# Robot wrist

- Rotates the object in an arbitrary orientation
- Three rotational joints (RRR)
  - Sometimes also one or two suffice
  - Links should be as short as possible



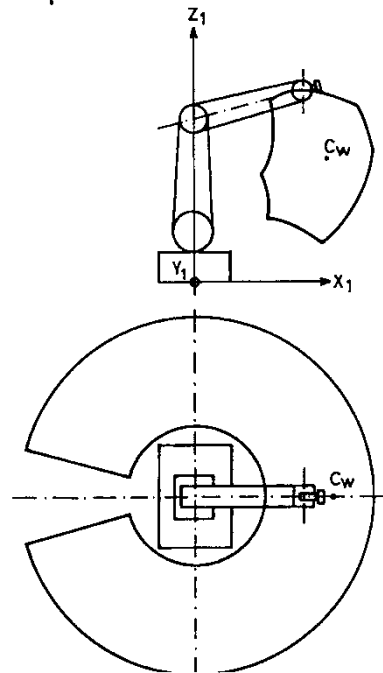
# Robot end-effector

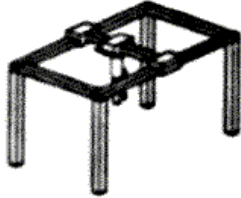
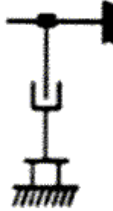
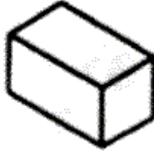
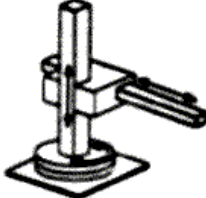


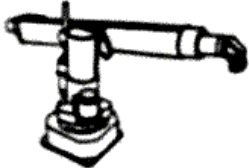


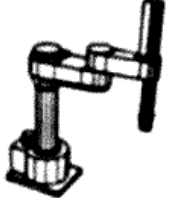
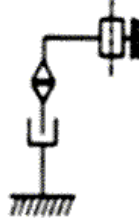




- The final link of the robot manipulator
  - Grippers with fingers
    - With two fingers
    - With more than two fingers
  - Other type of grippers
    - Vacuum
    - Magnetic
    - Perforation
  - Other tools as end-effectors
    - Welding gun
    - Spray painting gun



# Robot workspace

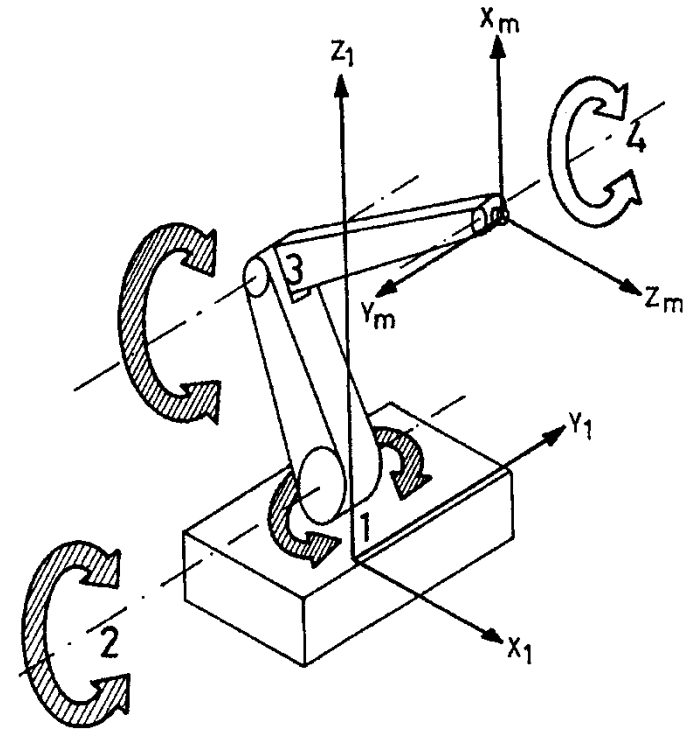
- Reachable workspace
  - The end-effector can reach every point in this space
- Dexterous workspace
  - The end-effector can reach every point in this space from the arbitrary orientation



Principle	Kinematic Structure	Workspace
 <p>Cartesian Robot</p>		
 <p>Cylindrical Robot</p>		
 <p>Spherical Robot</p>		
 <p>SCARA Robot</p>		
 <p>Articulated Robot</p>		

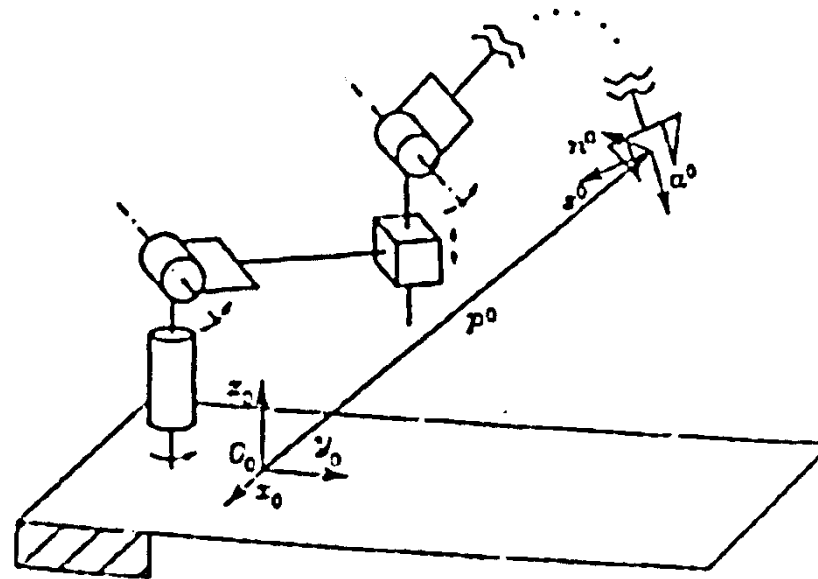
# Kinematics

- Base coordinate frame  $[X_1, Y_1, Z_1]$ 
  - Usually also world coordinate frame
  - Used for defining of the robotic task
- End-effector reference frame  $[X_m, Y_m, Z_m]$
- End-effector position
  - Vector between the origins of the coordinate frames
- Object orientation
  - Three angles
- Internal robot coordinates / joint variables
  - Joint states (angles, translations)
  - Uniquely describe the pose of the robot
- Direct kinematics
  - Determine the external robot coordinates from the internal coordinates
- Inverse kinematics
  - Determine the internal robot coordinates from the external coordinates



# Geometrical robot model

- Robot manipulator = a serial chain of segments connected by joints
- Every joint can be either rotational or translational
  - 1DOF – 1 internal coordinate



- Geometrical robot model describes
  - the pose of the last segment of the robot (end-effector) expressed in the reference (base) frame
  - depending on the current internal coordinates

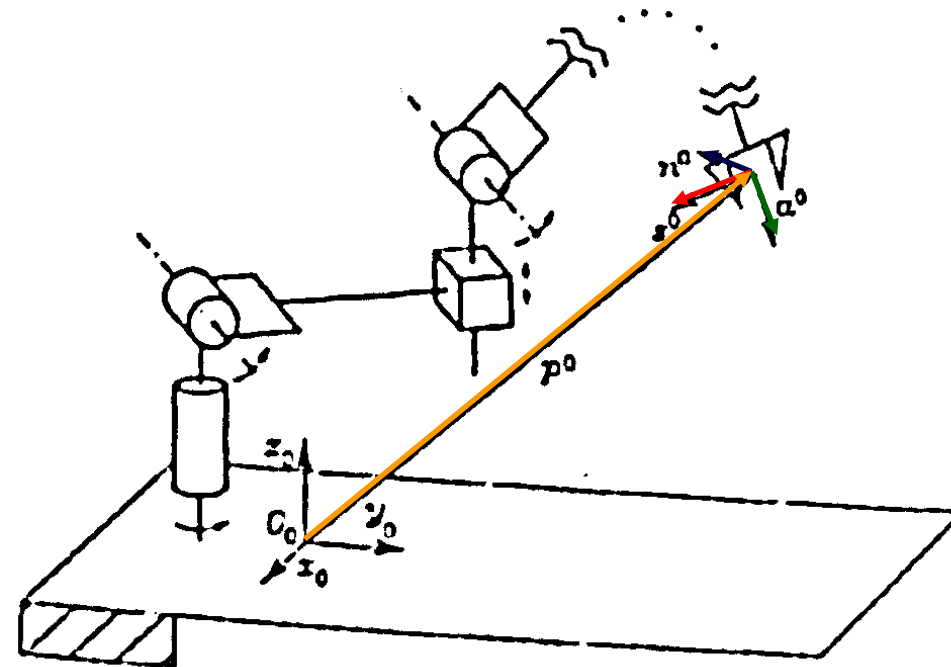


# Geometrical robot model

- Geometrical model can be expressed by a homogenous transformation:

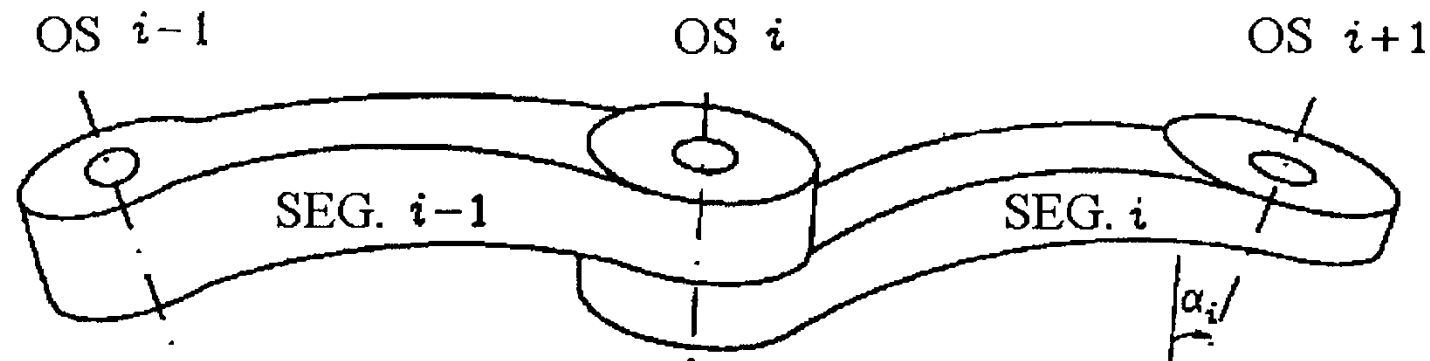
$$\mathbf{T}^o(\mathbf{q}) = \begin{bmatrix} \mathbf{n}^o(\mathbf{q}) & \mathbf{s}^o(\mathbf{q}) & \mathbf{a}^o(\mathbf{q}) & \mathbf{p}^o(\mathbf{q}) \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- $\mathbf{p}$  : position of the end effector in the reference coordinate frame
- $\mathbf{n}, \mathbf{s}, \mathbf{a}$  : unit vectors of the end-effector coordinate frame:
  - $\mathbf{a}$ : approach
  - $\mathbf{s}$ : sliding
  - $\mathbf{n}$ : normal
- $\mathbf{q}$  : vector of internal coordinates



# Poses of segments

- Every joint connects two neighbouring segments/links
  - Determine the transformation between them
  - Recursively build the full model for the entire robot
- Coordinate frames can be arbitrarily attached to the individual segments
- Denavit – Hartenberg rules simplify computation of the geometrical robot model
  - Determine the pose of the  $i$ -th c.f. with respect to the pose of the  $(i-1)$ -th c.f.
  - Axis  $i$  connects segments  $(i-1)$  and  $i$

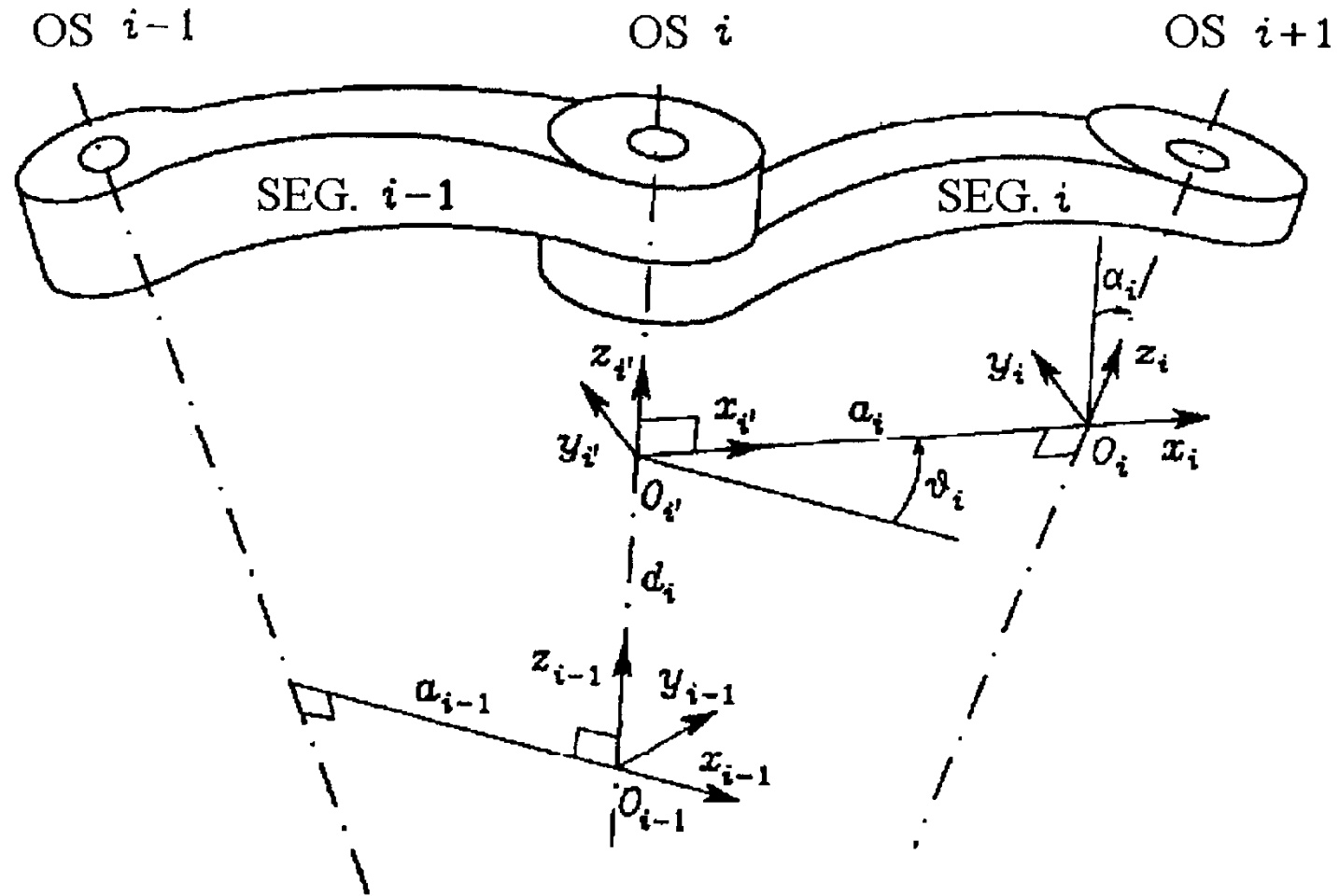


# Denavit – Hartenberg rules

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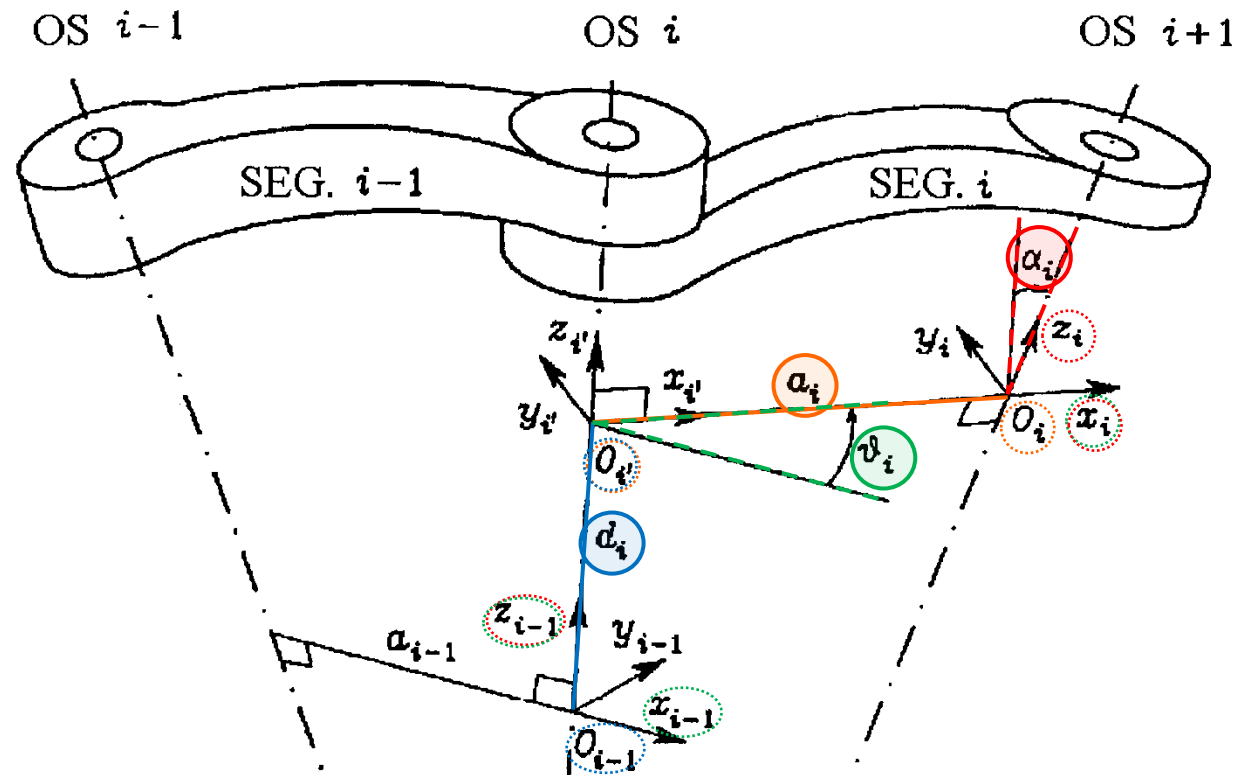
- Describe the coordinate frame of the  $i$ -th segment (having the joint  $i+1$ ):
  1. Define the axis  $z_i$  through the axis of the joint  $i+1$
  2. Find the common normal, perpendicular to the axes  $z_{i-1}$  and  $z_i$ 
    - Position the origin of  $O_i$  into the intersection of the axis  $z_i$  with the common normal
    - Position the origin of  $O_{i-1}$  into the intersection of the axis  $z_{i-1}$  with the common normal
    - If the axes are parallel, position the origin anywhere
  3. Position the axis  $x_i$  on a common normal in a way, that it is oriented from the joint  $i$  towards the joint  $i+1$ 
    - If the axis  $z_{i-1}$  and  $z_i$  intersect, orient the axis  $x_i$  perpendicular to the plane defined by the axes  $z_{i-1}$  in  $z_i$
  4. Determine the axis  $y_i$  in a way that gives the right-handed c.f.
  
- Similarly we also describe (have already described) the coordinate frame of the segment  $(i-1)$ 
  - The origin  $O_{i-1}$  is determined by the intersection of the common normal of the axes  $i-1$  and  $i$
  - The axis  $z_{i-1}$  is oriented along the  $i$ -th axis
  - $x_{i-1}$  is oriented along the common normal and directed from the joint  $i-1$  towards the joint  $i$

# Graphical illustration of DH parameters

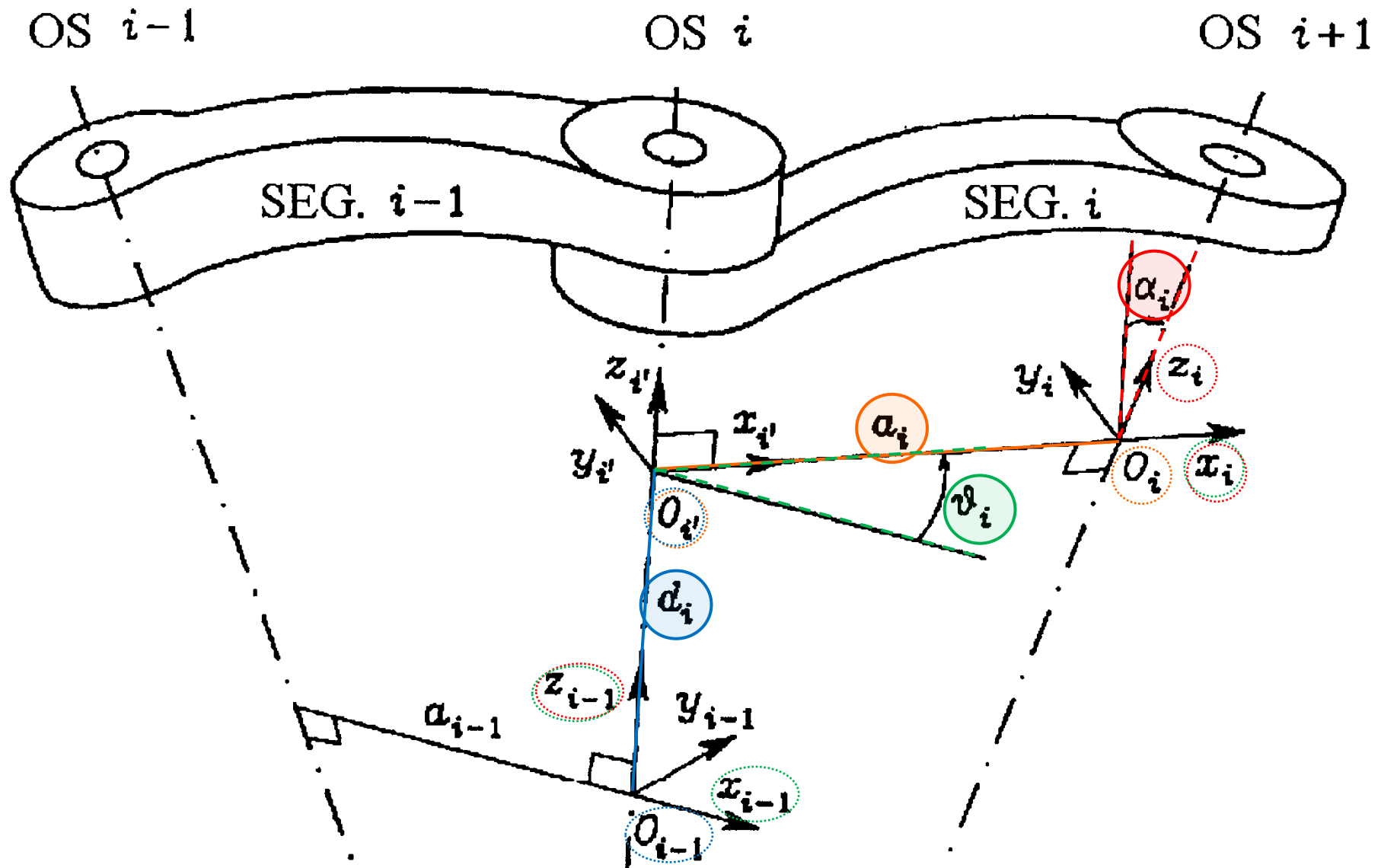


# Denavit – Hartenberg parameters

- The pose of  $i$ -th c.f. with respect to  $(i-1)$ -th c.f. is determined by 4 parameters:
  1.  $a_i$  – distance between  $O_i$  and  $O_{i'}$  along  $x_i$
  2.  $d_i$  – distance between  $O_{i-1}$  and  $O_{i'}$  along  $z_{i-1}$
  3.  $\alpha_i$  – angle between  $z_{i-1}$  and  $z_i$  around  $x_i$
  4.  $\theta_i$  – angle between  $x_{i-1}$  and  $x_i$  around  $z_{i-1}$



# Denavit – Hartenberg parameters



# Denavit – Hartenberg parameters

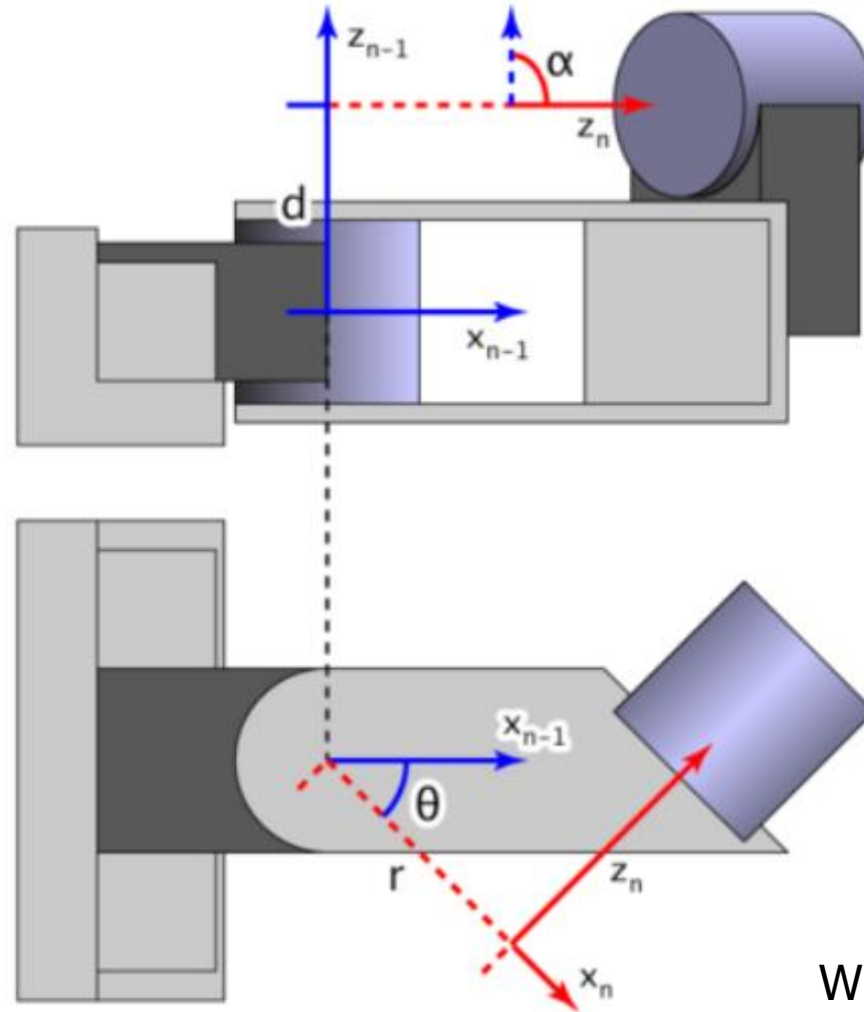
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- $a_i$  and  $\alpha_i$  are always constant
  - They depend on the geometry of the robot, the links between the joints, etc.
  - They do not change during the operation of the robot
- One of the two remaining parameters is a variable
  - $\Theta_i$ , if the  $i$ -th joint is rotational
  - $d_i$ , if the  $i$ -th joint is translational

# Denavit – Hartenberg parameters

- Illustration

- $r=a$
- $n=i$



Wikipedia

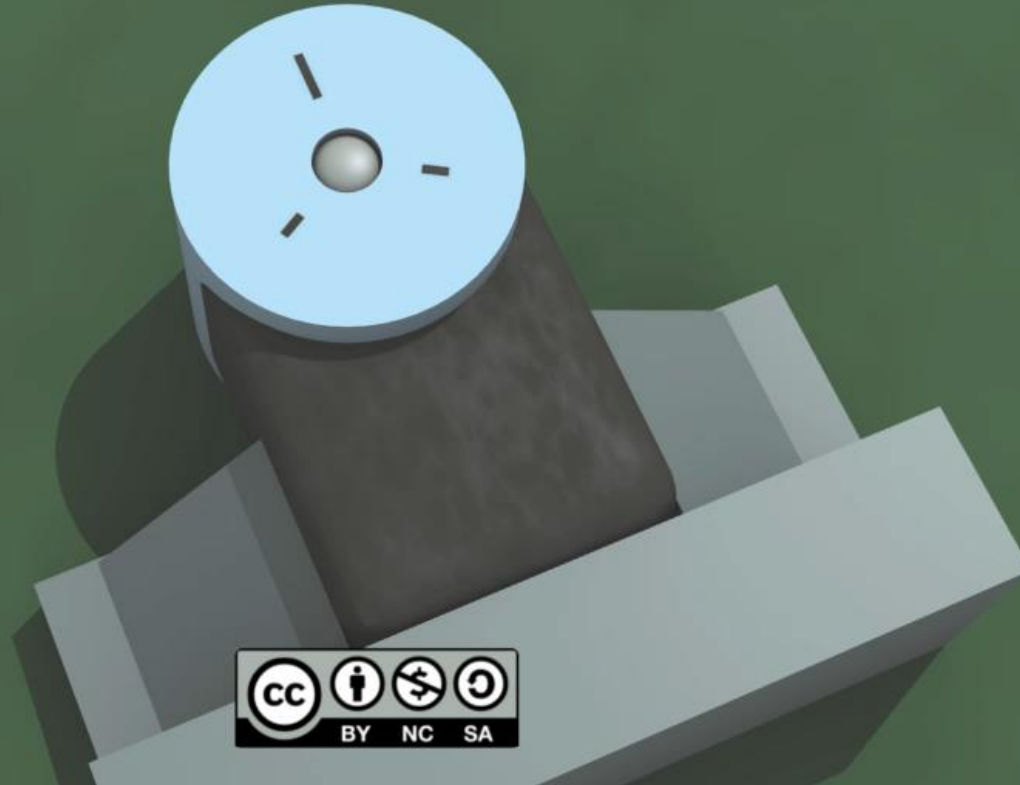


# Denavit – Hartenberg parameters

- Video:

## Denavit–Hartenberg Reference Frame Layout

Produced by Ethan Tira–Thompson



[http://en.wikipedia.org/wiki/Denavit-Hartenberg\\_Parameters](http://en.wikipedia.org/wiki/Denavit-Hartenberg_Parameters)

# Exceptions

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- Some exceptions in certain situations can be used to simplify the process:
  - Axis  $z_i$  and  $z_{i-1}$  are parallel  $\rightarrow d_i=0$
  - Axis  $z_i$  and  $z_{i-1}$  intersect  $\rightarrow O_i$  is in the intersection
  - In case of the base (0-th) segment: only the axis  $z_0$  is defined
    - $\rightarrow$  put the origin of  $O_0$  in the first joint
    - $\rightarrow$  align  $x_0$  and  $x_1$
  - In case of end-effector (n-th c.f.):  
Only axis  $x_n$  is defined; it is perpendicular to  $z_{n-1}$ 
    - $\rightarrow z_n$  should be parallel to  $z_{n-1}$
  - In case of translational joint:
    - $\rightarrow$  orient the axis  $z_{i-1}$  in the direction of translation
    - $\rightarrow$  position  $O_{i-1}$  at the beginning of translation

# Denavit – Hartenberg transformation

- Transformation between the i-th and (i-1)-th c.f.:

1. Take the c.f.  $O_{i-1}$  attached to the segment (i-1)

2. Translate it for  $d_i$  and rotate it for  $\Theta_i$  along and around  $z_{i-1}$ , to align it with the c.f.  $O_i$ .

3. Translate c.f.  $O_i$  for  $a_i$  in rotate it for  $\alpha_i$  along and around  $x_i$ , to align it with the c.f.  $O_i$ .

4. DH transformation is obtained by postmultiplication of both transformation matrices

- Function of a single variable:
  - $\Theta_i$  for rotational joint
  - $d_i$  for translational joint

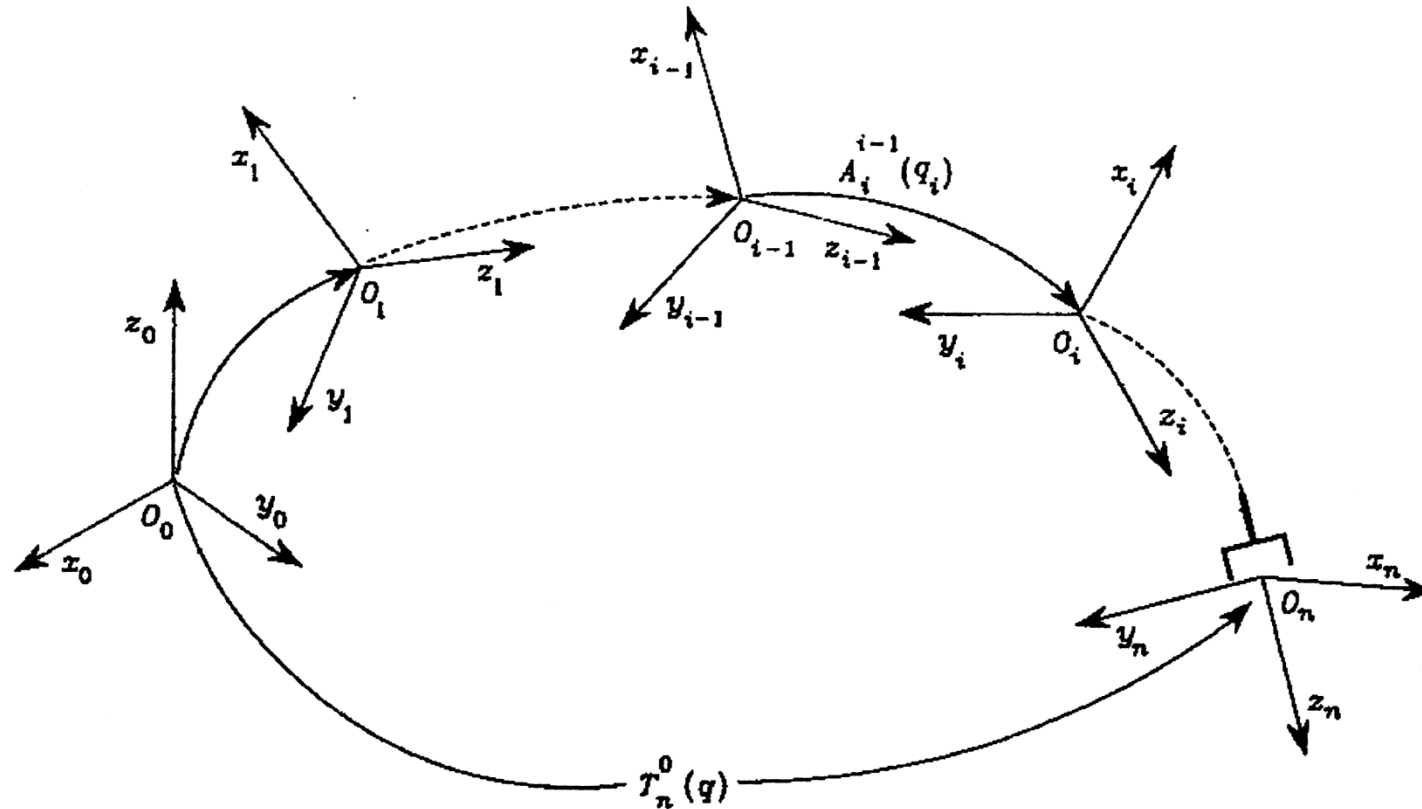
$$\mathbf{A}_i^{i-1} = \begin{bmatrix} c\theta_i & -s\theta_i & 0 & 0 \\ s\theta_i & c\theta_i & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_i^{i'} = \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & c\alpha_i & -s\alpha_i & 0 \\ 0 & s\alpha_i & c\alpha_i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_i^{i-1}(q_i) = \mathbf{A}_i^{i-1} \cdot \mathbf{A}_i^{i'} = \begin{bmatrix} c\theta_i & -s\theta_i c\alpha_i & s\theta_i s\alpha_i & a_i c\theta_i \\ s\theta_i & c\theta_i c\alpha_i & -c\theta_i s\alpha_i & a_i s\theta_i \\ 0 & s\alpha_i & c\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

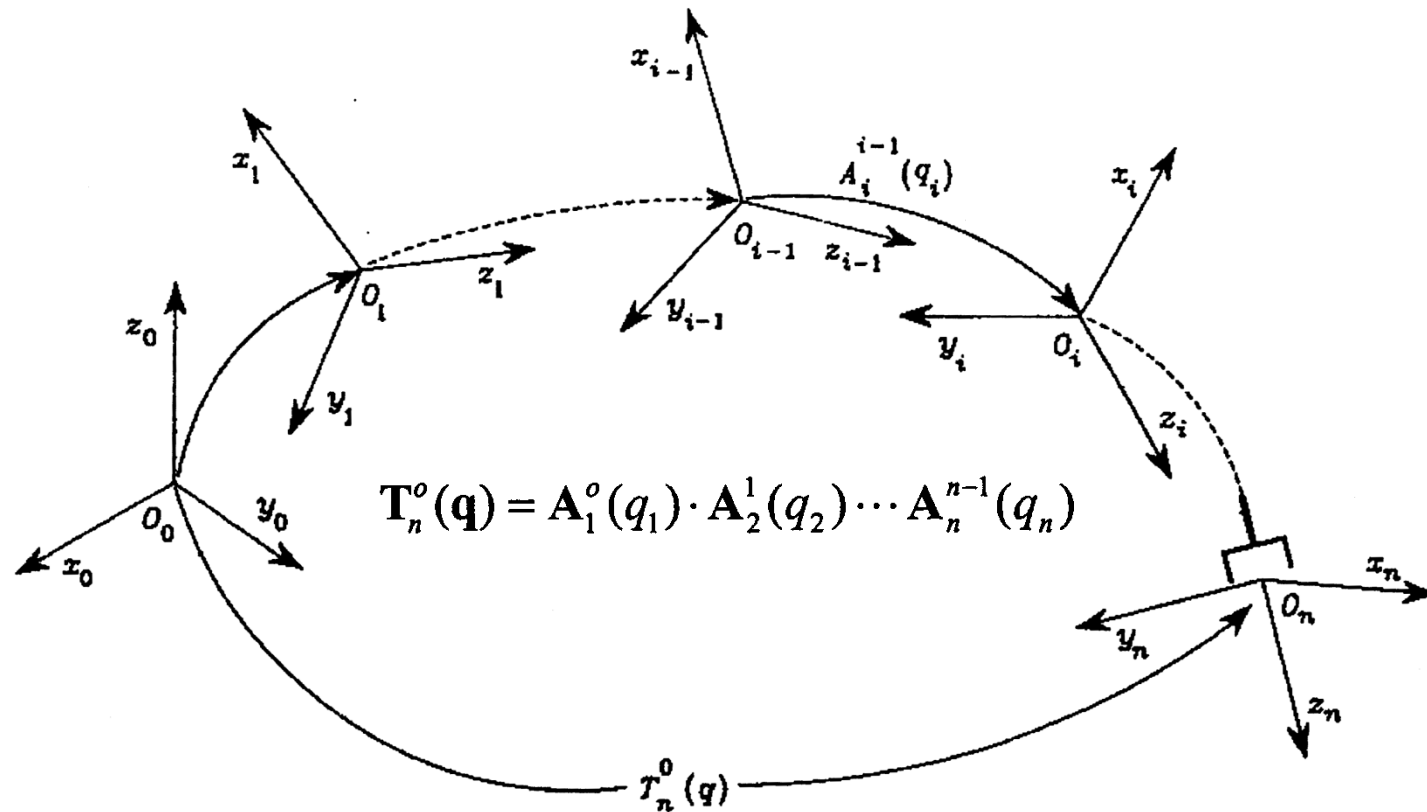
# Calculation of the geometrical robot model

1. Set the coordinate frames for all segments
2. Define the table of DH parameters  $a_i, d_i, \alpha_i$  in  $\theta_i$  for all segments  $i=1,2,\dots,n$
3. Calculate DH transformations  $A_i^{i-1}(q_i)$  for  $i=1,2,\dots,n$
4. Calculate the geometrical model:  $T_n^0(\mathbf{q}) = A_1^0(q_1) \cdot A_2^1(q_2) \cdots A_n^{n-1}(q_n)$

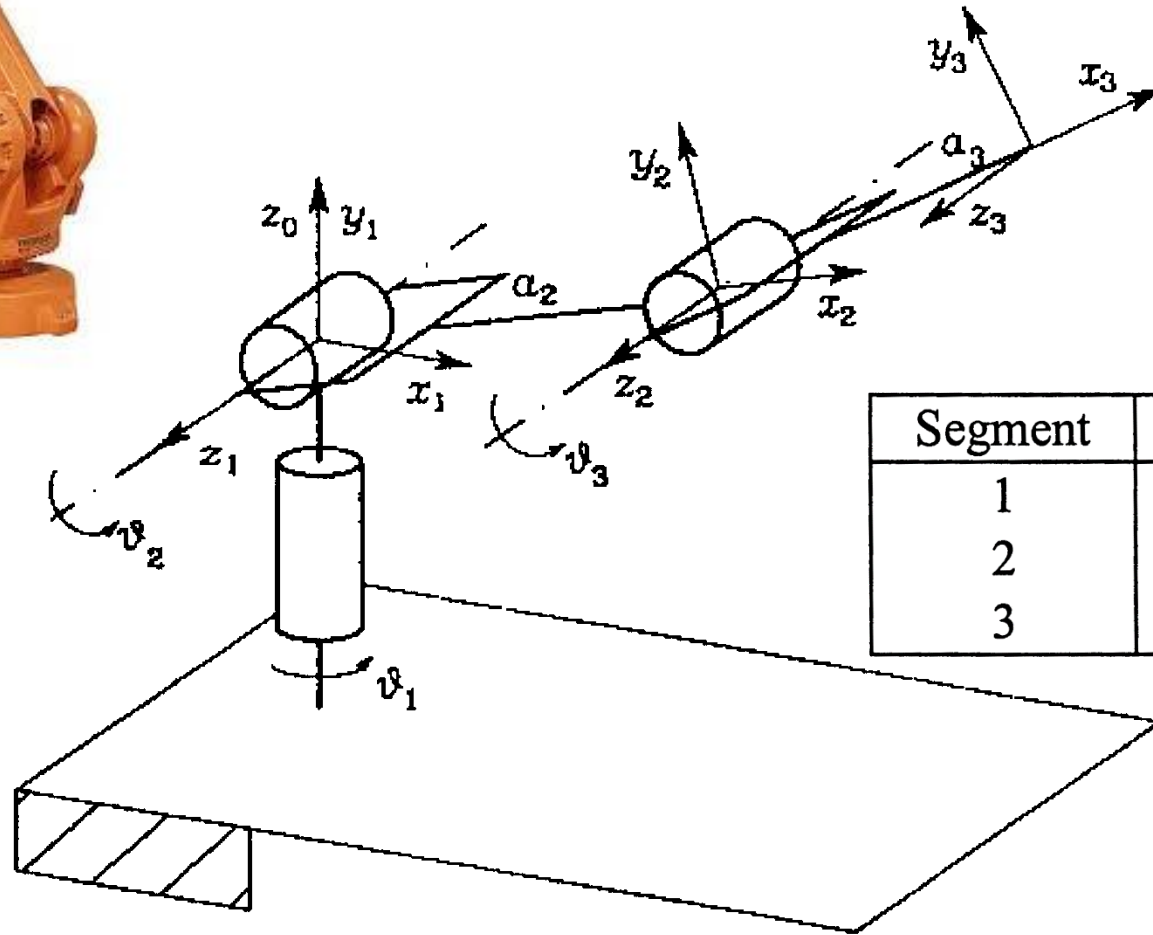


# Using geometrical model

- Geometrical robot model gives the pose of the last segment of the robot (end-effector) expressed in the reference (base) frame
- Geometrical robot model defines the pose (position and orientation) of the end-effector depending on the current internal coordinates  $\mathbf{q}$



# Anthropomorphic robot manipulator



Segment	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	$\pi/2$	0	$\theta_1$
2	$a_2$	0	0	$\theta_2$
3	$a_3$	0	0	$\theta_3$

$$\mathbf{q} = [\theta_1, \theta_2, \theta_3]^T$$

# Anthropomorphic robot manipulator

Segment	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	$\pi/2$	0	$\theta_1$
2	$a_2$	0	0	$\theta_2$
3	$a_3$	0	0	$\theta_3$

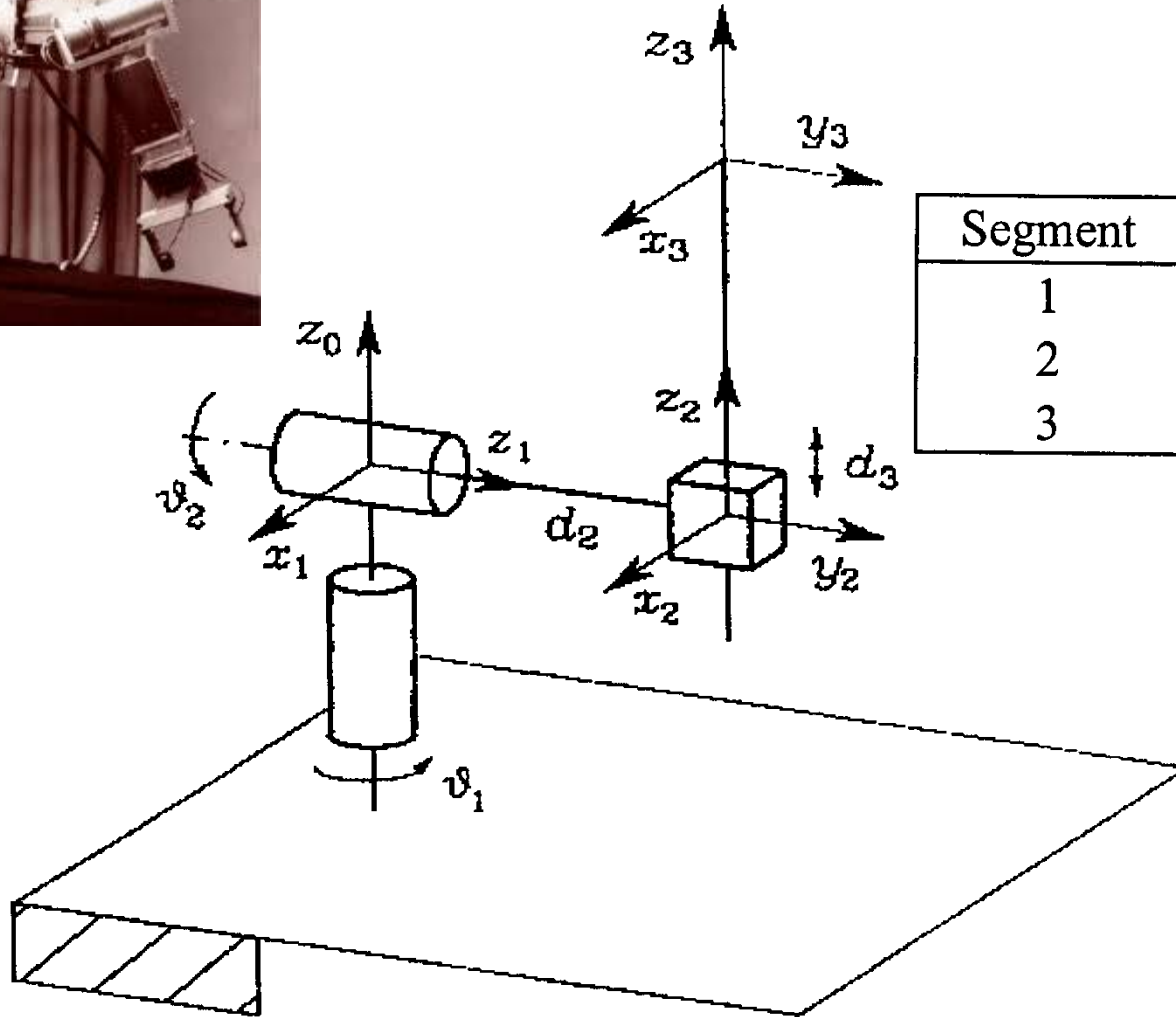
$$\mathbf{A}_i^{i-1}(q_i) = \begin{bmatrix} c\theta_i & -s\theta_i c\alpha_i & s\theta_i s\alpha_i & a_i c\theta_i \\ s\theta_i & c\theta_i c\alpha_i & -c\theta_i s\alpha_i & a_i s\theta_i \\ 0 & s\alpha_i & c\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_1^0(\theta_1) = \begin{bmatrix} c_1 & 0 & s_1 & 0 \\ s_1 & 0 & -c_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_i^{i-1}(\theta_i) = \begin{bmatrix} c_i & -s_i & 0 & a_i c_i \\ s_i & c_i & 0 & a_i s_i \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad i=2,3$$

$$\mathbf{T}_3^0(\mathbf{q}) = \mathbf{A}_1^0 \cdot \mathbf{A}_2^1 \cdot \mathbf{A}_3^2 = \begin{bmatrix} c_1 c_{23} & -c_1 s_{23} & s_1 & c_1 (a_2 c_2 + a_3 c_{23}) \\ s_1 c_{23} & -s_1 s_{23} & -c_1 & s_1 (a_2 c_2 + a_3 c_{23}) \\ s_{23} & c_{23} & 0 & a_2 s_2 + a_3 s_{23} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Stanford robot manipulator



Segment	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	$-\pi/2$	0	$\theta_1$
2	0	$\pi/2$	$d_2$	$\theta_2$
3	0	0	$d_3$	0

$$\mathbf{q} = [\theta_1, \theta_2, d_3]^T$$



# Stanford robot manipulator

Segment	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	$-\pi/2$	0	$\theta_1$
2	0	$\pi/2$	$d_2$	$\theta_2$
3	0	0	$d_3$	0

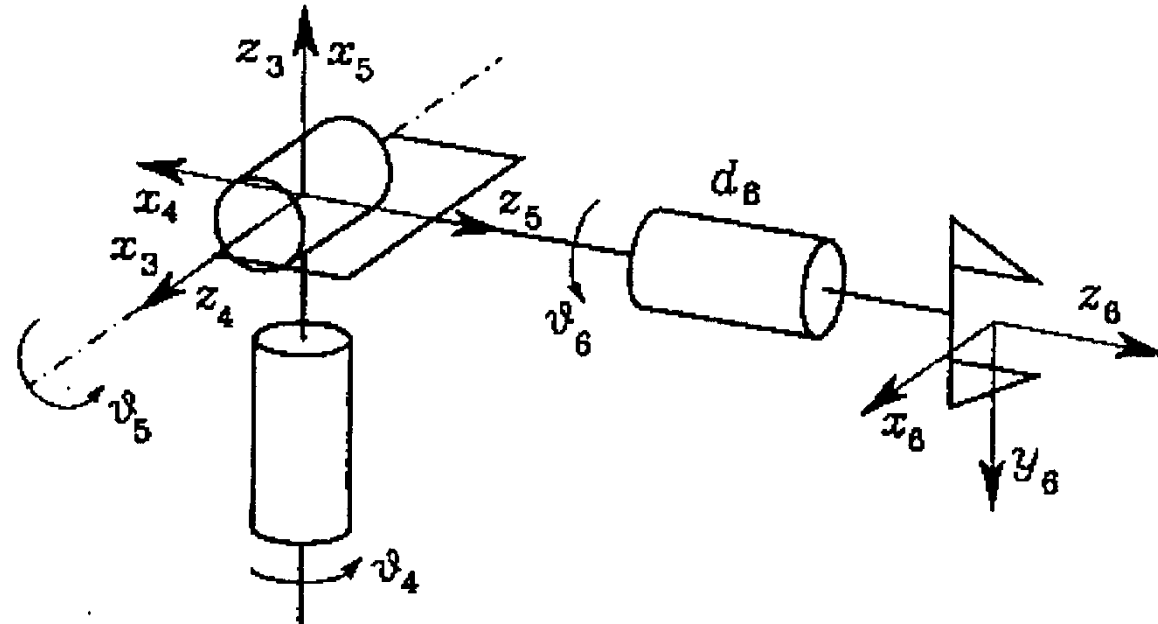
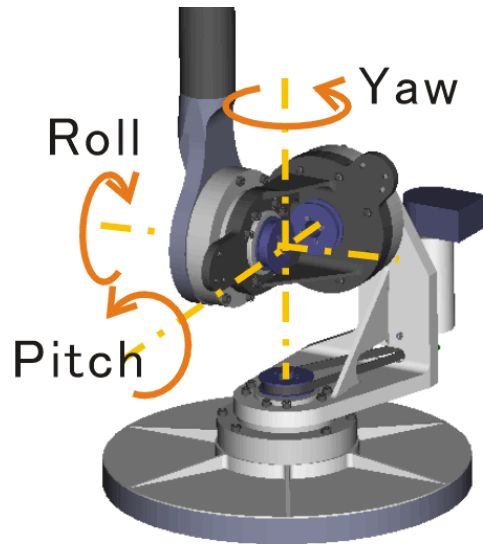
$$\mathbf{q} = [\theta_1, \theta_2, d_3]^T$$

$$\mathbf{A}_1^0(\theta_1) = \begin{bmatrix} c_1 & 0 & -s_1 & 0 \\ s_1 & 0 & c_1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{A}_2^1(\theta_2) = \begin{bmatrix} c_2 & 0 & s_2 & 0 \\ s_2 & 0 & -c_2 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{A}_3^2(d_3) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{T}_3^0(\underline{q}) = \mathbf{A}_1^0 \cdot \mathbf{A}_2^1 \cdot \mathbf{A}_3^2 = \begin{bmatrix} c_1 c_2 & -s_1 & c_1 s_2 & c_1 s_2 d_3 - s_1 d_2 \\ s_1 c_2 & c_1 & s_1 s_2 & s_1 s_2 d_3 + c_1 d_2 \\ -s_2 & 0 & c_2 & c_2 d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Spherical robot wrist

- Usually attached to the end of the robot arm



- All three axes of the rotational joints intersect in the same point

$$\mathbf{q} = [\theta_4, \theta_5, \theta_6]^T$$

Segment	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
4	0	$-\pi/2$	0	$\theta_4$
5	0	$\pi/2$	0	$\theta_5$
6	0	0	$d_6$	$\theta_6$

# Spherical robot wrist

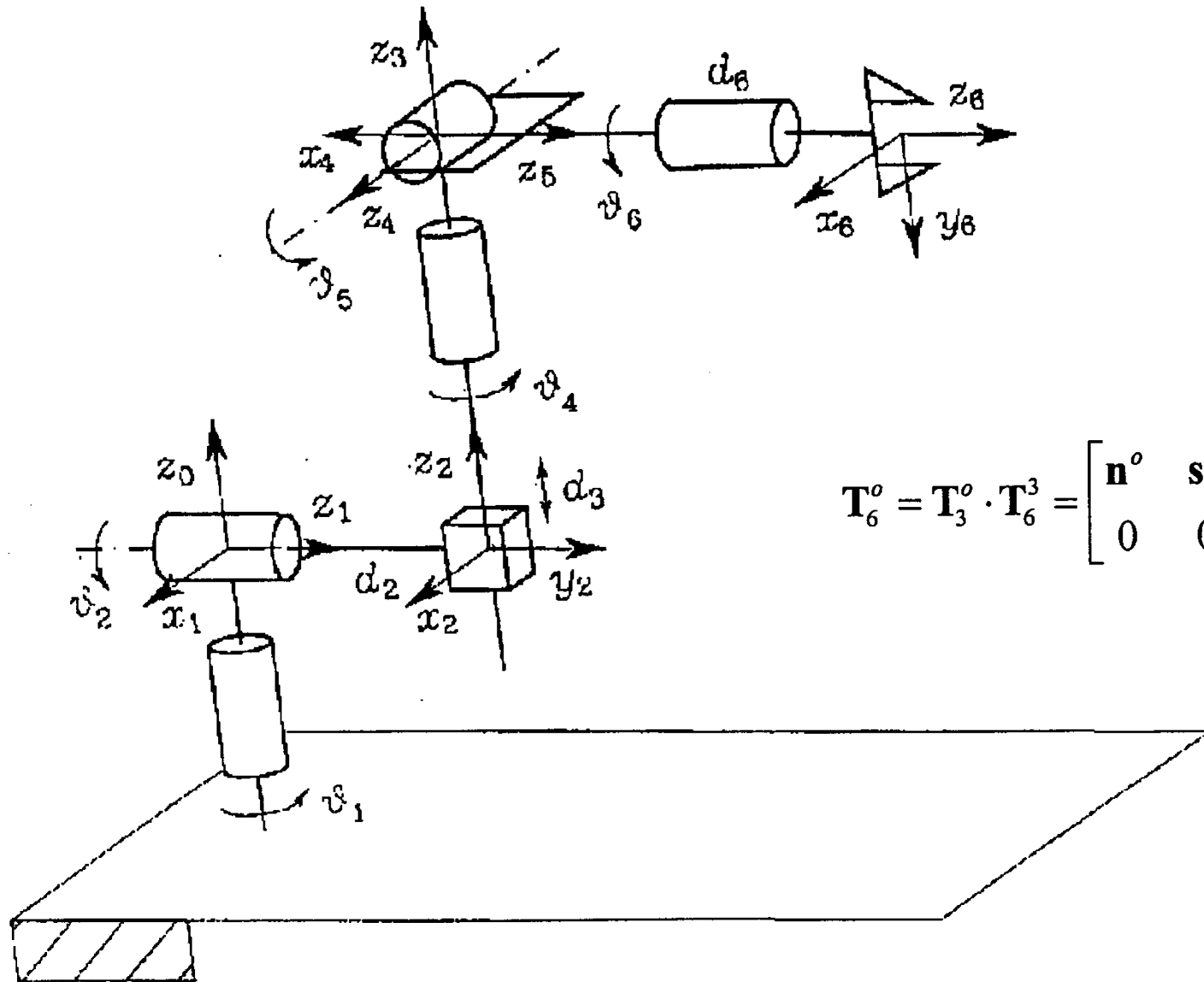
Segment	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
4	0	$-\pi/2$	0	$\theta_4$
5	0	$\pi/2$	0	$\theta_5$
6	0	0	$d_6$	$\theta_6$

$$\mathbf{q} = [\theta_4, \theta_5, \theta_6]^T$$

$$\mathbf{A}_4^3(\theta_4) = \begin{bmatrix} c_4 & 0 & -s_4 & 0 \\ s_4 & 0 & c_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{A}_5^4(\theta_5) = \begin{bmatrix} c_5 & 0 & s_5 & 0 \\ s_5 & 0 & -c_5 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{A}_6^5(\theta_6) = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{T}_6^3(\underline{q}) = \mathbf{A}_4^3 \cdot \mathbf{A}_5^4 \cdot \mathbf{A}_6^5 = \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_4 c_6 & c_4 s_5 & c_4 s_5 d_6 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & s_4 s_5 & s_4 s_5 d_6 \\ -s_5 c_6 & s_5 s_6 & c_5 & c_5 d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Stanford manipulator with the wrist



$$\mathbf{T}_6^0 = \mathbf{T}_3^0 \cdot \mathbf{T}_6^3 = \begin{bmatrix} \mathbf{n}^0 & \mathbf{s}^0 & \mathbf{a}^0 & \mathbf{p}^0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Stanford manipulator with the wrist

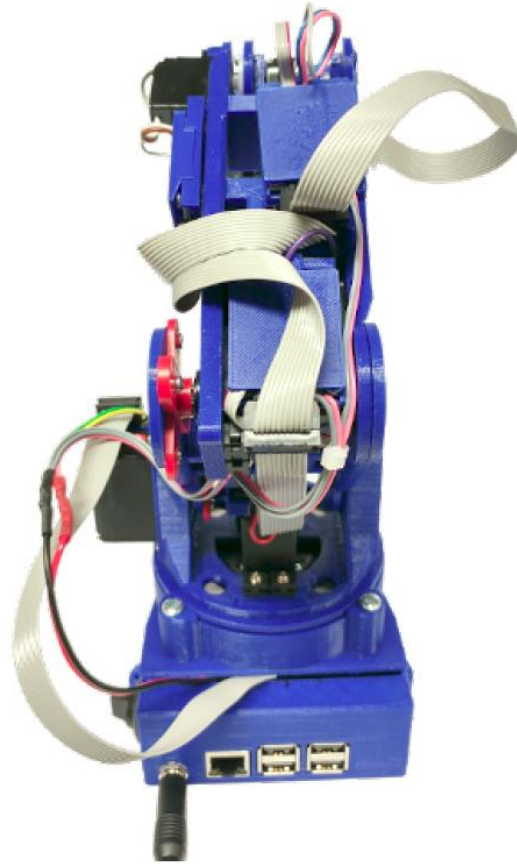
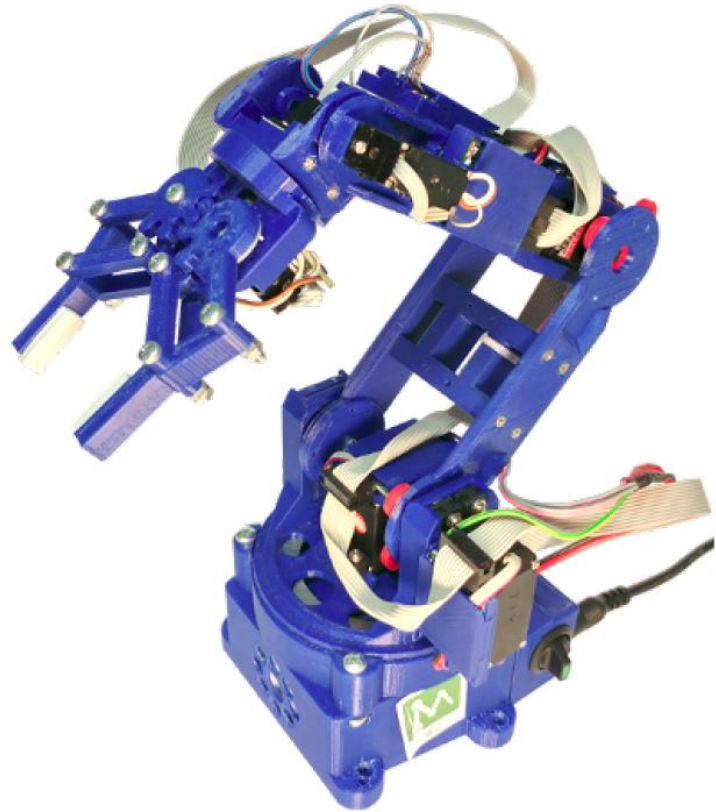
$$\mathbf{p}^o = \begin{bmatrix} c_1 s_2 d_3 - s_1 d_2 + (c_1 (c_2 c_4 s_5 + s_2 c_5) - s_1 s_4 s_5) d_6 \\ s_1 s_2 d_3 + c_1 d_2 + (s_1 (c_2 c_4 s_5 + s_2 c_5) + c_1 s_4 s_5) d_6 \\ c_2 d_3 + (-s_2 c_4 s_5 - c_2 c_5) d_6 \end{bmatrix}$$
$$\mathbf{n}^o = \begin{bmatrix} c_1 (c_2 (c_4 c_5 c_6 - s_4 s_6) - s_2 s_5 c_6) - s_1 (s_4 c_5 c_6 + c_4 s_6) \\ s_1 (c_2 (c_4 c_5 c_6 - s_4 s_6) - s_2 s_5 c_6) + c_1 (s_4 c_5 c_6 + c_4 s_6) \\ -s_2 (c_4 c_5 c_6 - s_4 s_6) - c_2 s_5 s_6 \end{bmatrix}$$
$$\mathbf{s}^o = \begin{bmatrix} c_1 (-c_2 (c_4 c_5 s_6 + s_4 c_6) + s_2 s_5 s_6) - s_1 (-s_4 c_5 c_6 + c_4 c_6) \\ s_1 (-c_2 (c_4 c_5 s_6 + s_4 c_6) + s_2 s_5 s_6) + c_1 (-s_4 c_5 c_6 + c_4 c_6) \\ s_2 (c_4 c_5 s_6 + s_4 c_6) + c_2 s_5 s_6 \end{bmatrix}$$
$$\mathbf{a}^o = \begin{bmatrix} c_1 (c_2 c_4 s_5 + s_2 c_5) - s_1 s_4 s_5 \\ s_1 (c_2 c_4 s_5 + s_2 c_5) + c_1 s_4 s_5 \\ -s_2 c_4 s_5 + c_2 c_5 \end{bmatrix}$$

# Inverse kinematics model

---

- Direct kinematics defines the pose of the end-effector depending on the internal coordinates
  - Where will the end-effector move  $\mathbf{T}(\mathbf{q})$
  - The pose of the end-effector is uniquely determined
- Inverse kinematics defines the internal coordinates that would bring the robot end-effector in the desired pose
  - How to move the end-effector to reach the desired pose
  - Challenging problem:  $\mathbf{q}(\mathbf{T})$ 
    - Nonlinear equations
    - The solution is not uniquely defined
      - Several solutions
      - Sometimes even infinite number of solutions
      - Sometimes the solution does not exist
  - Take into account several criteria that determine which solution is optimal
  - Sometimes we can get analytical solution, sometimes only numerical are possible

# ViCoS LCLWOS robot manipulator



# Requirements



## Low production cost

The cost of a single unit should be below 300€, it should use widely available components where possible.



## Easy construction and maintenance

Construction from parts should be simple, parts should be easily replaceable.



## Simplicity and ease of use

The interaction with the platform should be multi-level



## Robustness

Both the hardware and software should be robust enough to withstand long-term use.



## Safety

The manipulator should be safe enough to be operated even by kids.



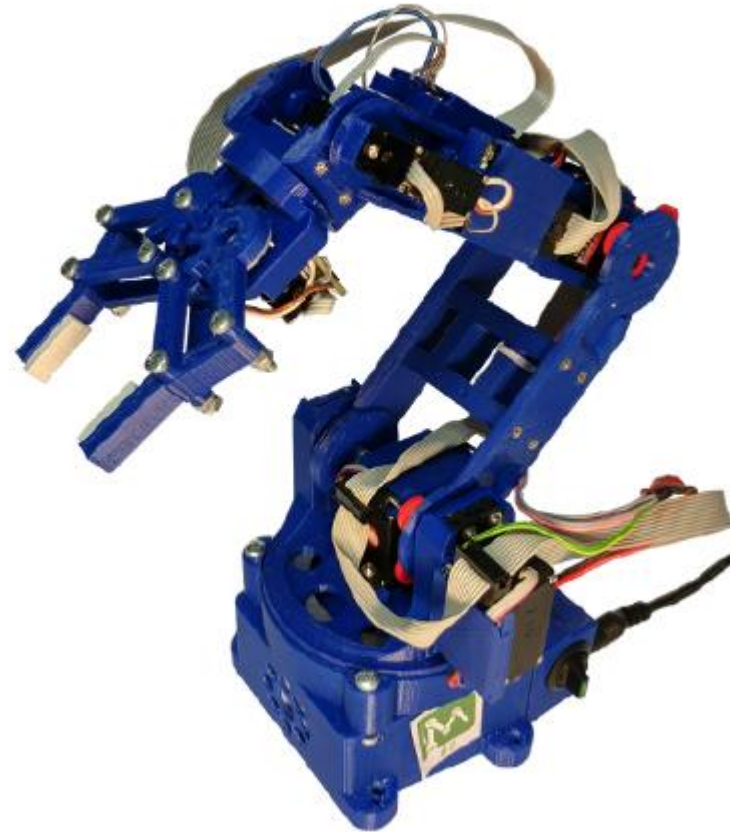
## Realism

The experience should be real enough for students of different university-level courses on robotics.



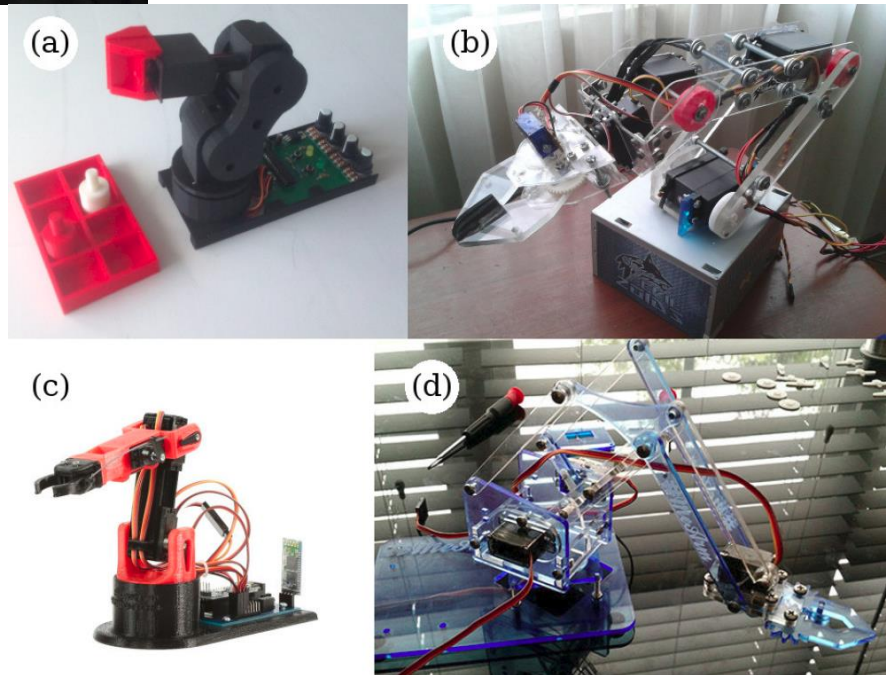
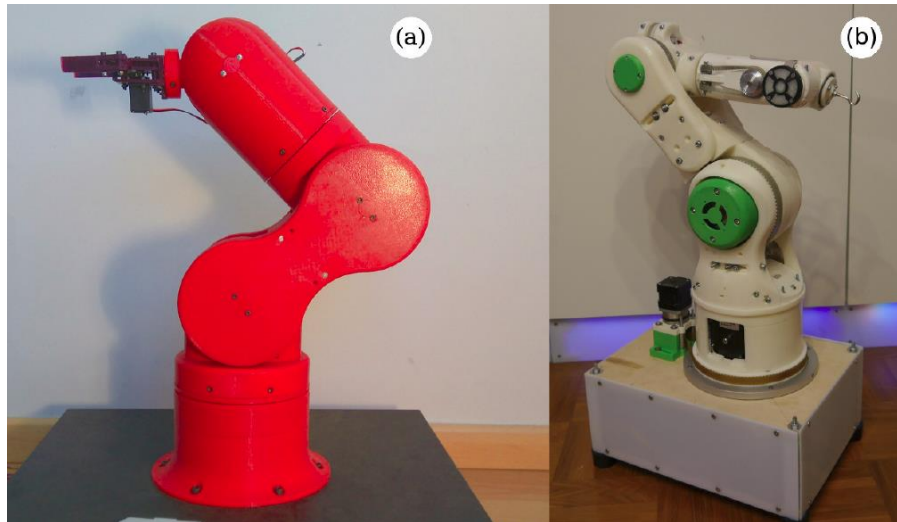
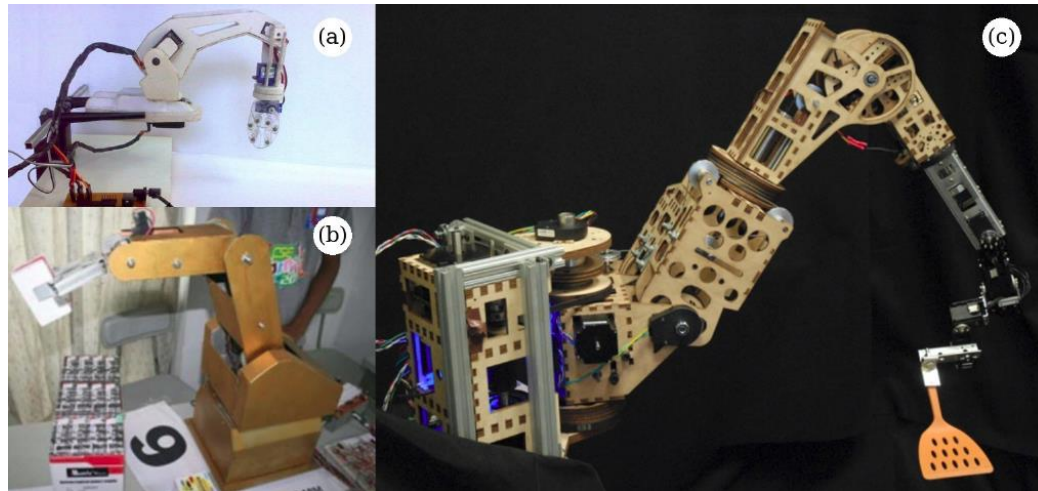
## Openness

Both the hardware designs and software sources should be available for others to

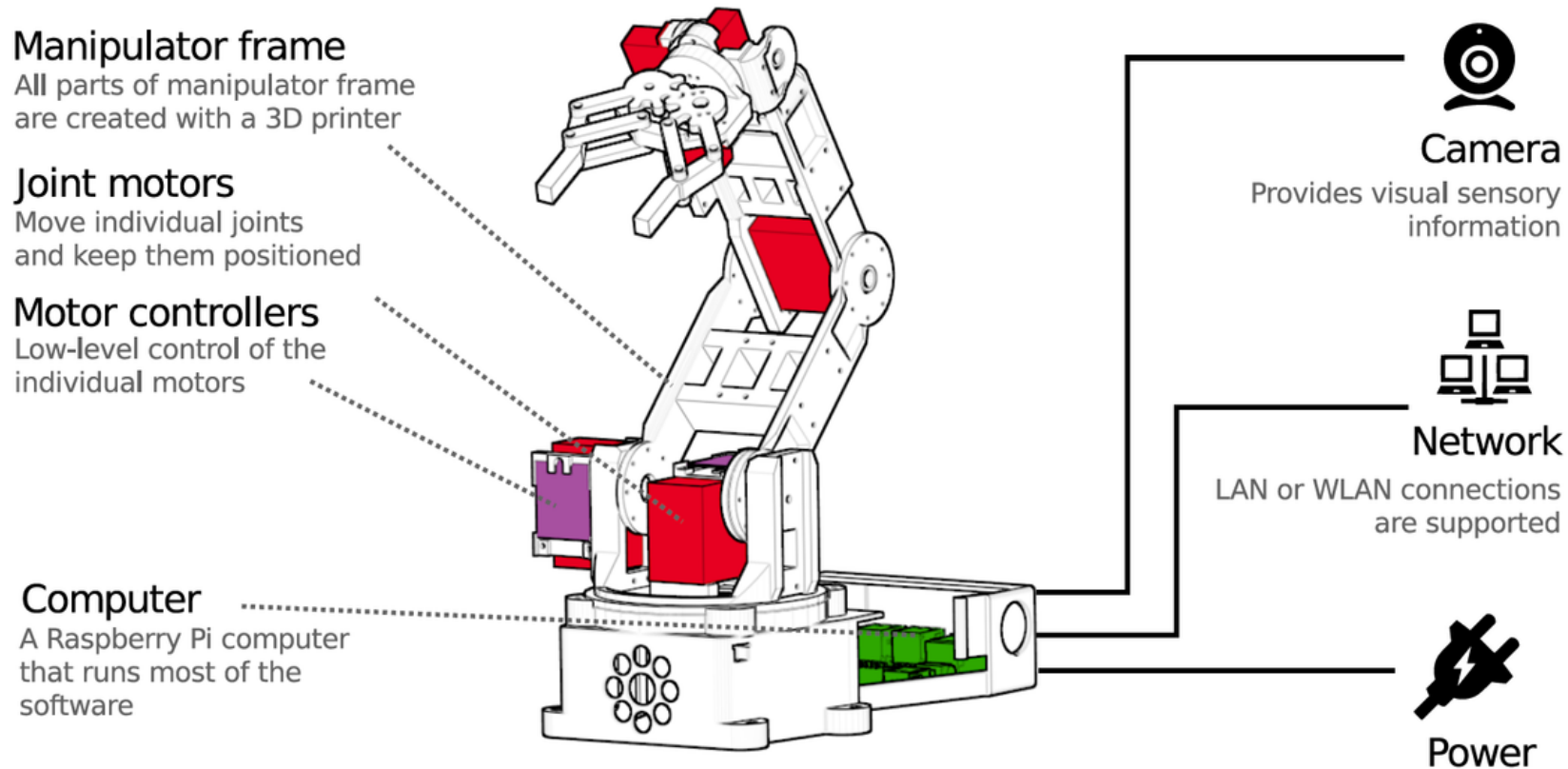




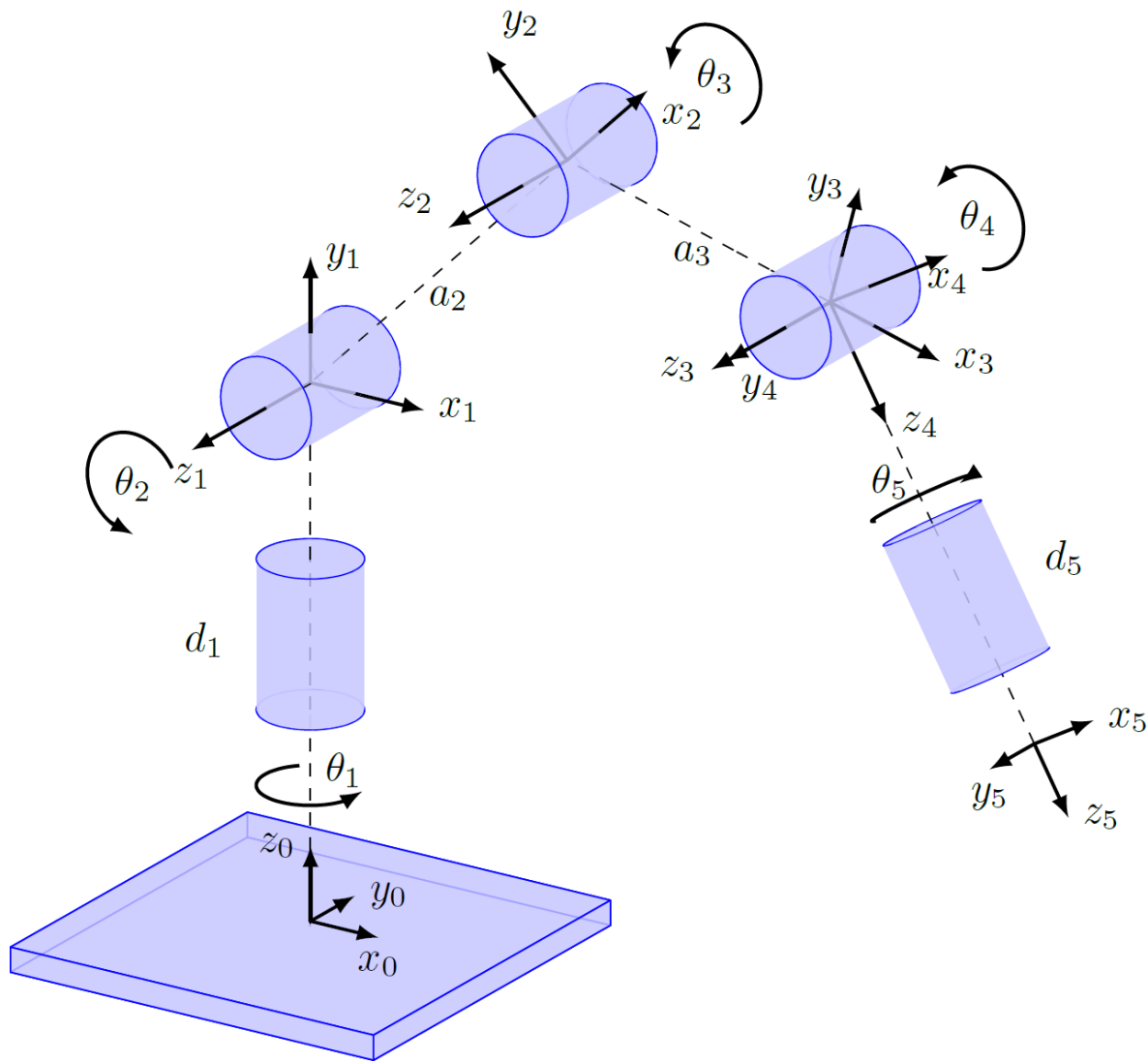
# Related work



# Robot manipulator



# Forward model



DH parameters:

Segment	$a_i$	$d_i$	$\alpha_i$	$\theta_i$
1	0 mm	48 mm	$90^\circ$	$\theta_1$
2	108 mm	0 mm	$0^\circ$	$\theta_2$
3	112 mm	0 mm	$0^\circ$	$\theta_3$
4	0 mm	0 mm	$90^\circ$	$\theta_4$
5	0 mm	90 mm	$0^\circ$	$\theta_5$

# Transformation

$$A_i^{i-1} = \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cos \alpha_i & \sin \theta_i \sin \alpha_i & a_i \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cos \alpha_i & -\cos \theta_i \sin \alpha_i & a_i \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3^2 = \begin{bmatrix} \cos \theta_3 & -\sin \theta_3 & 0 & a_3 \cos \theta_3 \\ \sin \theta_3 & \cos \theta_3 & 0 & a_3 \sin \theta_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_1^0 = \begin{bmatrix} \cos \theta_1 & 0 & \sin \theta_1 & 0 \\ \sin \theta_1 & 0 & -\cos \theta_1 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_4^3 = \begin{bmatrix} \cos \theta_4 & 0 & \sin \theta_4 & 0 \\ \sin \theta_4 & 0 & -\cos \theta_4 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

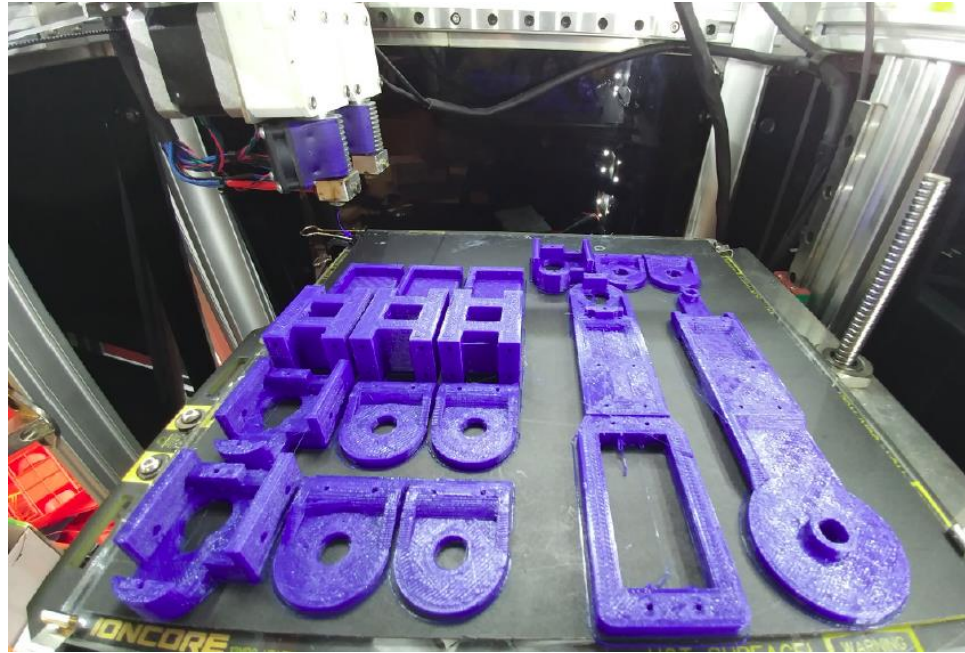
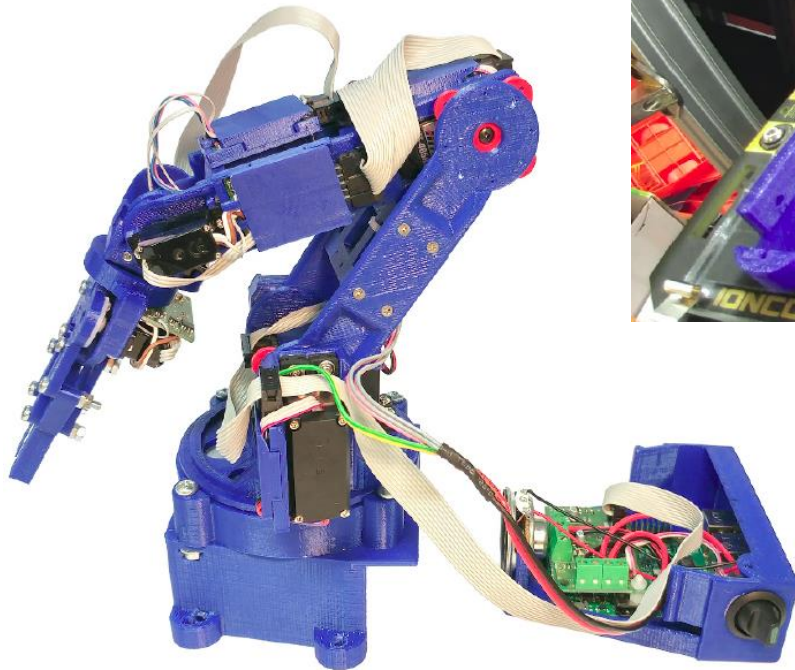
$$A_2^1 = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & a_2 \cos \theta_2 \\ \sin \theta_2 & \cos \theta_2 & 0 & a_2 \sin \theta_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_5^4 = \begin{bmatrix} \cos \theta_5 & -\sin \theta_5 & 0 & 0 \\ \sin \theta_5 & \cos \theta_5 & 0 & 0 \\ 0 & 0 & 1 & d_5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_5^0 = A_1^0 A_2^1 A_3^2 A_4^3 A_5^4$$

# Frame

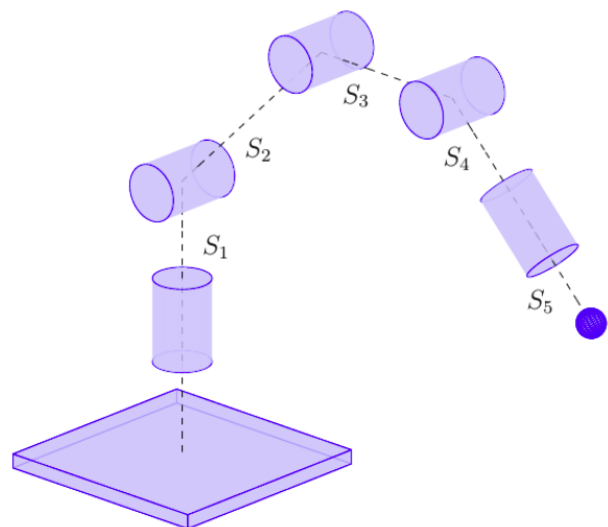
- 3D printed





# Motors

- Servo motors



Sklep	Servomotor
S1	HS-311
S2	HS-645MG
S3	HS-485HB
S4	ES08AII
S5	ES08AII
Prijemalo	ES08AII

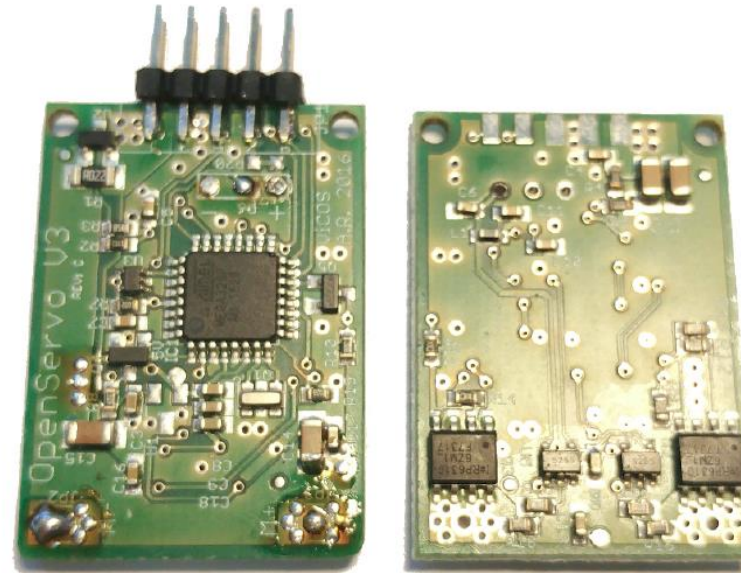
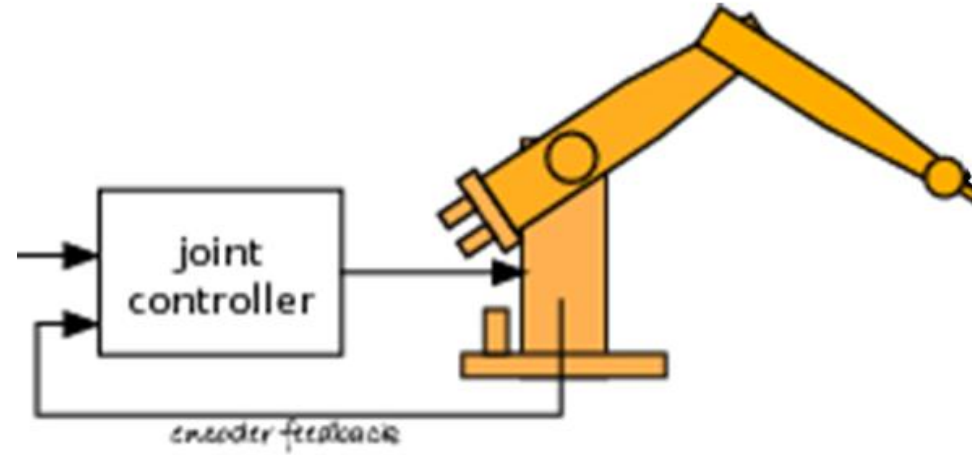
# Motors

Servo- motor	Nape- tost	Rotacijska hitrost	Navor	Kratko- stični tok	Teža	Material zobnikov
HS- 645MG	4,8 V	0,24 s/60°	7,7 kg/cm	2,5 A	55,2 g	kovina
	6,0 V	0,20 s/60°	9,6 kg/cm			
HS- 485HB	4,8 V	0,22 s/60°	4,8 kg/cm	1,2 A	45,0 g	karbonit
	6,0 V	0,20 s/60°	6,0 kg/cm			
HS-311	4,8 V	0,19 s/60°	3,0 kg/cm	0,8 A	43,0 g	najlon
	6,0 V	0,15 s/60°	3,5 kg/cm			
ES08AII	4,8 V	0,12 s/60°	1,5 kg/cm	0,7 A	8,5 g	najlon
	6,0 V	0,10 s/60°	1,8 kg/cm			



# Upgrading servomotors

- New control circuit
- Potentiometer
- OpenServo
- Current protection



# PID controller

- Proportional, integral and derivative part

$$u(t_k) = K_p e(t_k) + K_i \sum_{n=1}^k e(t_n) \Delta t + \frac{e(t_k) - e(t_{k-1})}{\Delta t}$$

```
1: // Proporcionalni del
2: p_component = seek_position - current_position;
3: pwm_output = (int32_t)p_component * (int32_t)p_gain;
4: // Odvodni del
5: d_component = (p_component - p_component_old) * 256;
6: pwm_output+ = (int32_t)d_component * (int32_t)d_gain;
7: // Integralni del
8: i_component+ = p_component;
9: pwm_output+ = (((int32_t)i_component * (int32_t)i_gain) >> 8);
10: //
11: pwm = ((int16_t)(pwm_output >> 8));
```

Sklep	$K_p$	$K_i$	$K_d$
S1	500	300	5
S2	500	300	5
S3	500	300	5
S4	300	200	5
S5	150	200	5
Prijemalo	500	200	5

# AD converter

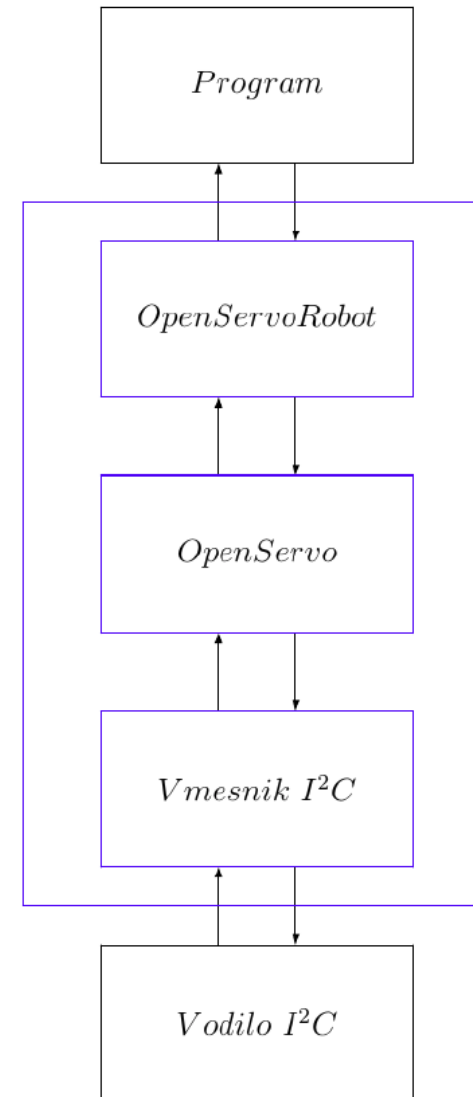
- Increasing resolution
- Multiple sampling and decimation
- Resolution increased from 10 to 12 bits
- Sampling frequency 256 Hz

$$ADC_{(10+n)bit} = \frac{\sum_{k=1}^{4^n} ADC_{10bit}}{2^n}$$

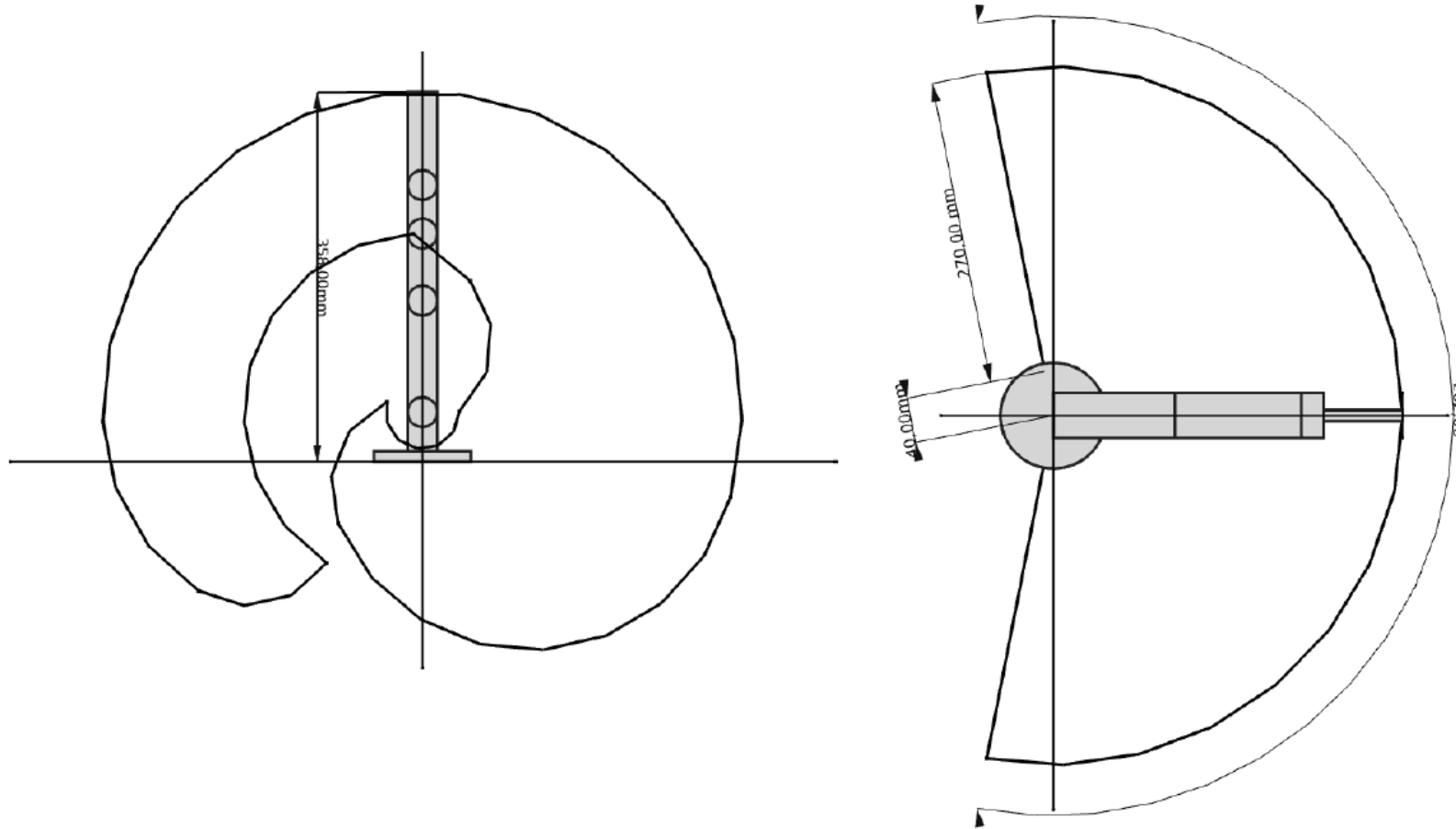
Ločljivost	Čas branja	Največja frekvenca
10 bitov	$\approx 0,0864 \text{ ms}$	$\approx 11574 \text{ Hz}$
11 bitov	$\approx 0,3456 \text{ ms}$	$\approx 2893 \text{ Hz}$
12 bitov	$\approx 1,3824 \text{ ms}$	$\approx 723 \text{ Hz}$
13 bitov	$\approx 5,5296 \text{ ms}$	$\approx 180 \text{ Hz}$

# Communication

- I<sup>2</sup>C interface
  - I<sup>2</sup>C bus
- OpenServo
  - Communication with microcontroller
- OpenServoRobot
  - Robot model (DH parameters)
  - Communication with application



# Workspace

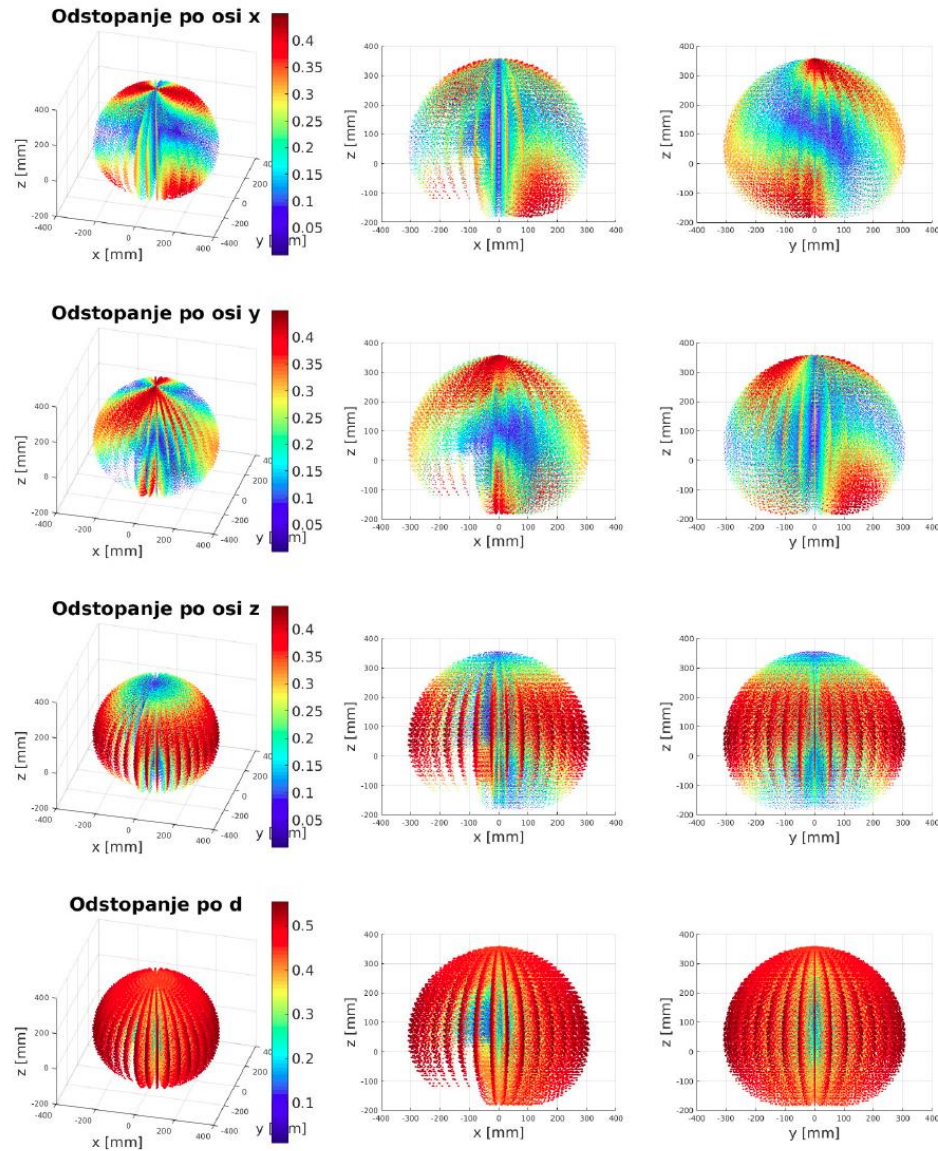


# Theoretical accuracy

- Expected deviation of the estimated position from the reference position of the end effector
- Only considering motor errors
- Theoretical upper limit of precision

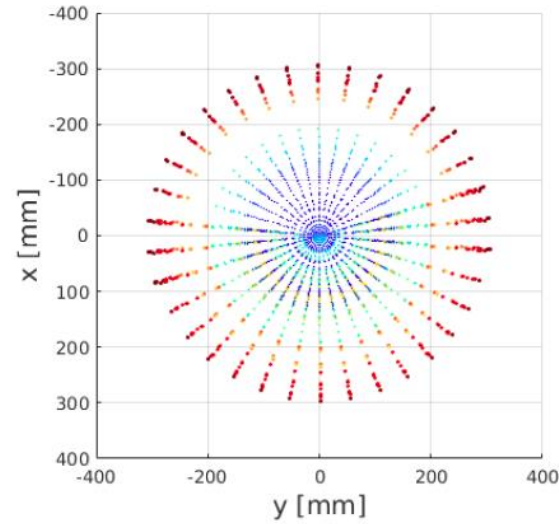
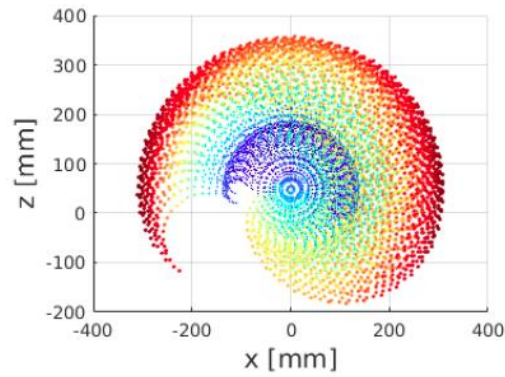
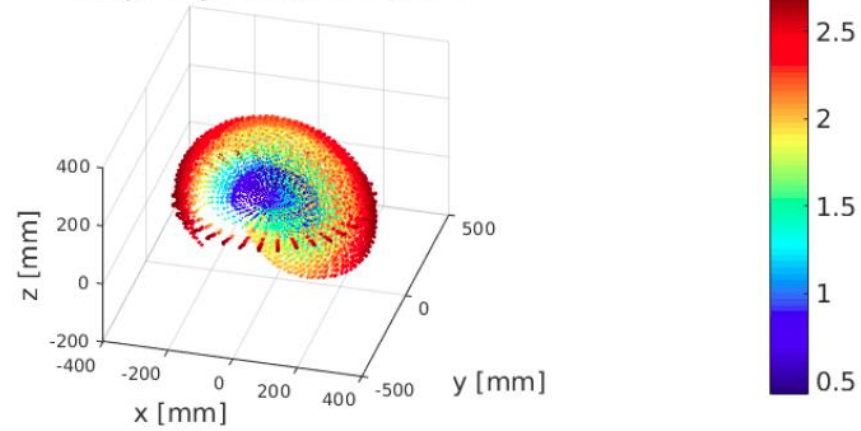
Osi	Odstopanje (mm)			Standardni odklon (mm)		
	Najmanj	Največ	Povprečno	Najmanj	Največ	Povprečno
x	0,00	0,45	0,14	0,01	0,61	0,20
y	0,00	0,45	0,14	0,00	0,61	0,21
z	0,00	0,44	0,16	0,03	0,56	0,66
d	0,10	0,55	0,29	0,14	0,73	0,41

# Theoretical accuracy



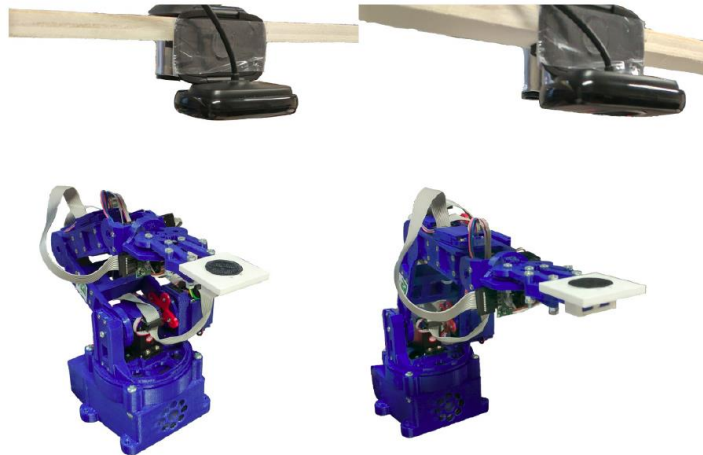
# Theoretical accuracy

Največja napaka po d

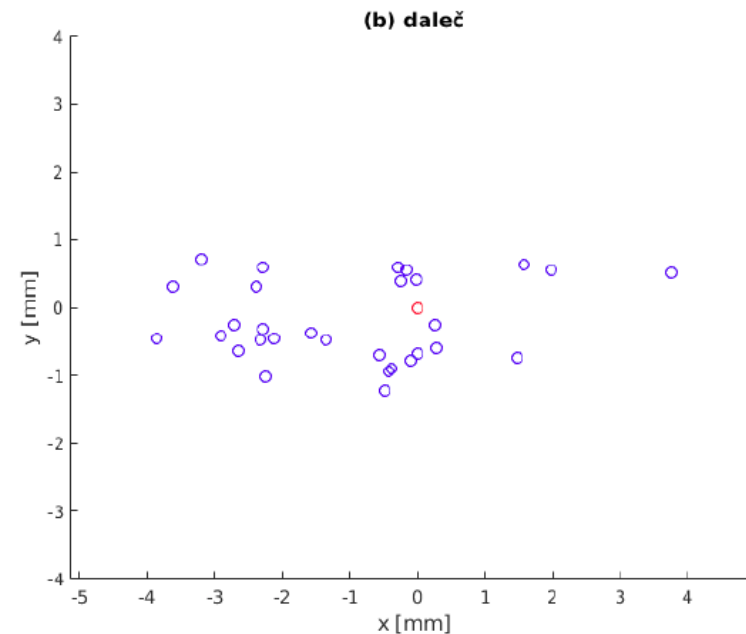
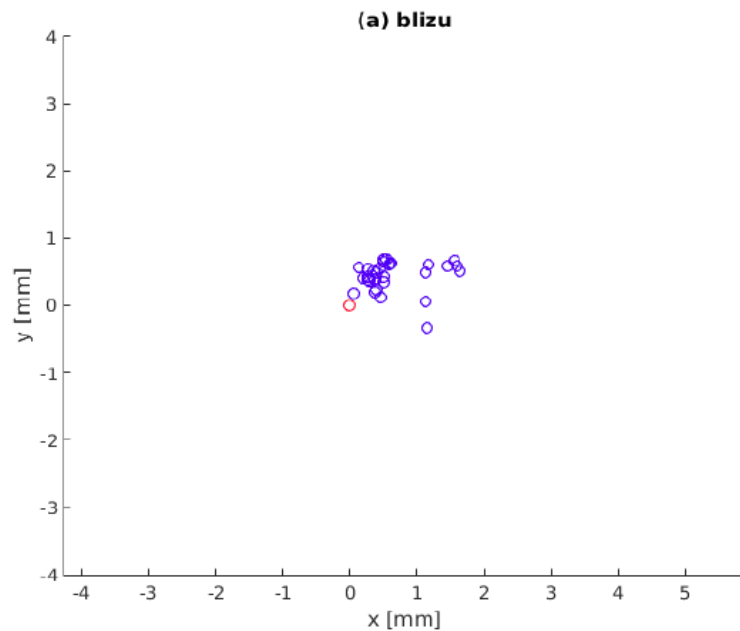




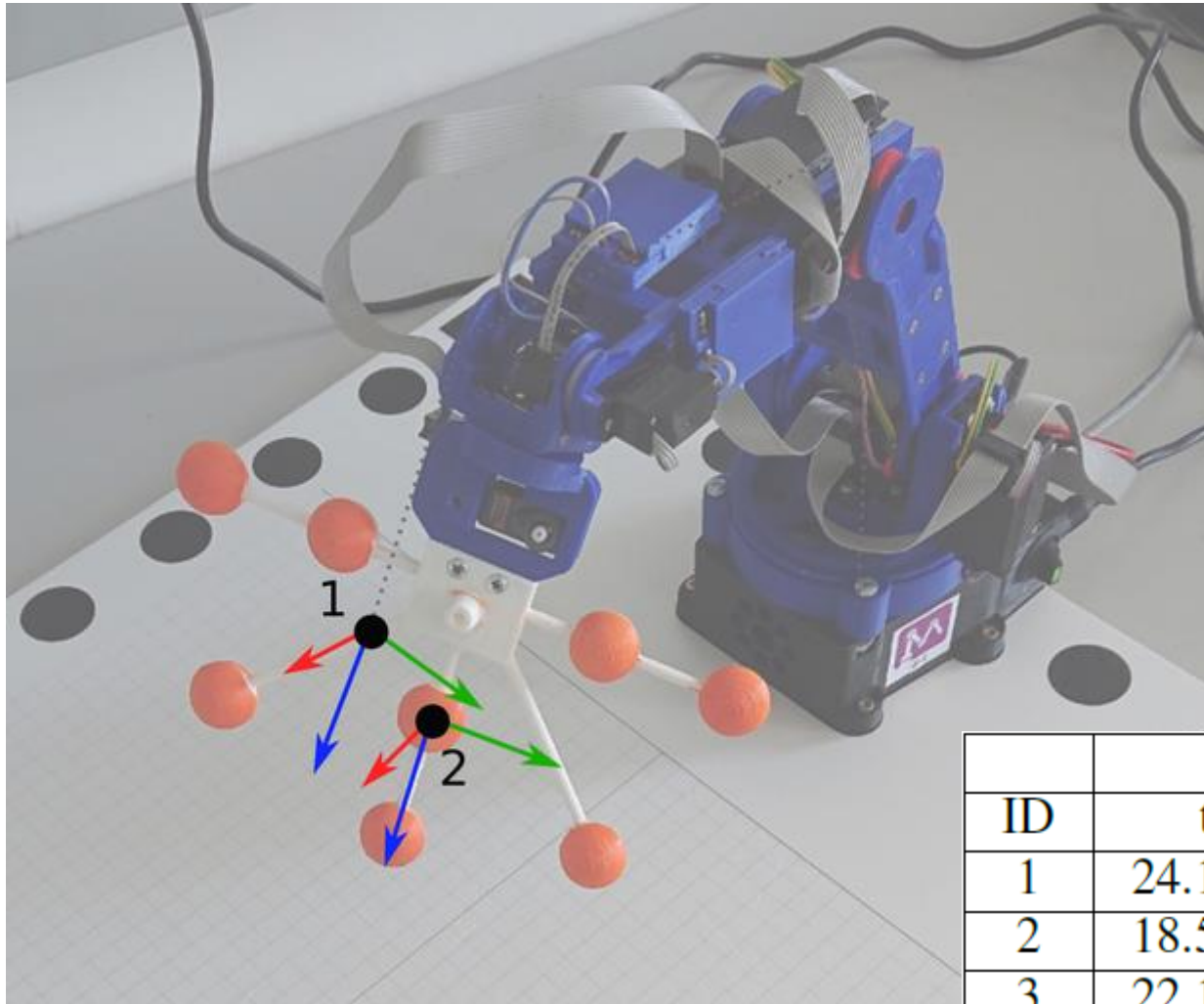
# Empirical repeatability



Meritev	Os x	Os y
Blizu	1,4 mm	0,6 mm
Daleč	3,8 mm	0,7 mm



# Calibration



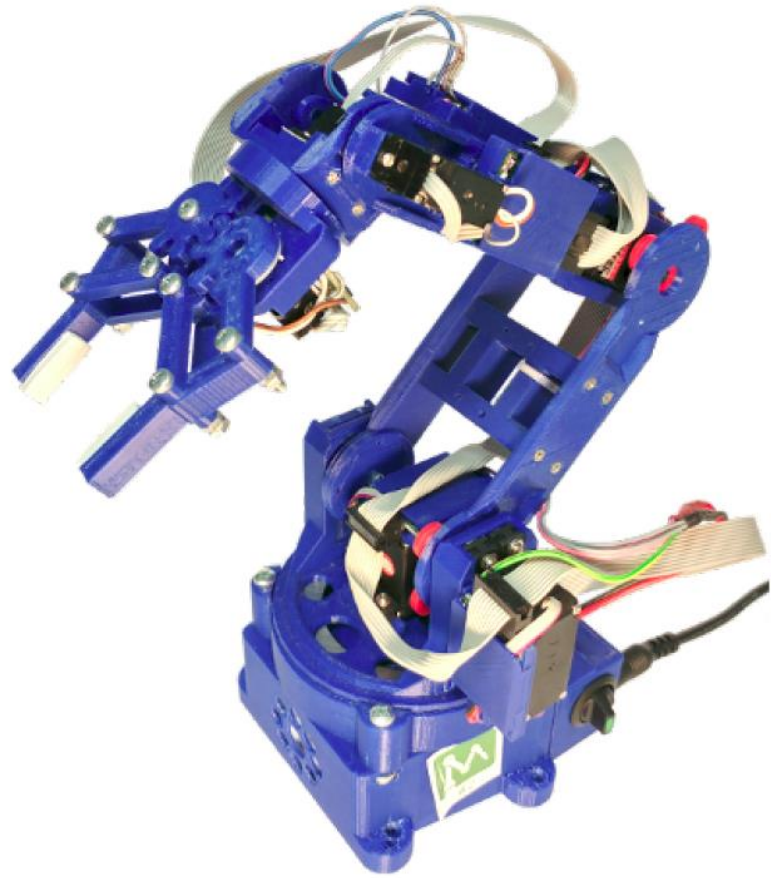
Grasping a cube (100 times):

ID	Uncalibrated	Calibrated
1	69	99
2	97	100
3	18	88
4	27	99

Mean error:

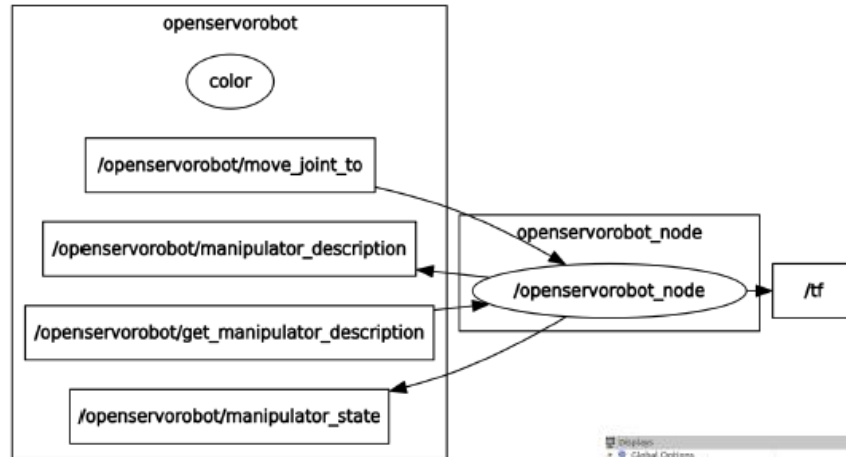
ID	Uncalibrated		Calibrated	
	train	test	train	test
1	$24.1 \pm 5.1$	$23.0 \pm 4.9$	$4.3 \pm 3.7$	$5.3 \pm 3.9$
2	$18.5 \pm 3.7$	$20.5 \pm 4.9$	$3.5 \pm 2.8$	$4.7 \pm 3.6$
3	$22.1 \pm 4.7$	$22.5 \pm 3.9$	$4.4 \pm 4.7$	$3.6 \pm 4.0$
4	$24.9 \pm 5.6$	$24.0 \pm 6.2$	$4.4 \pm 4.2$	$5.3 \pm 5.3$

# Characteristics

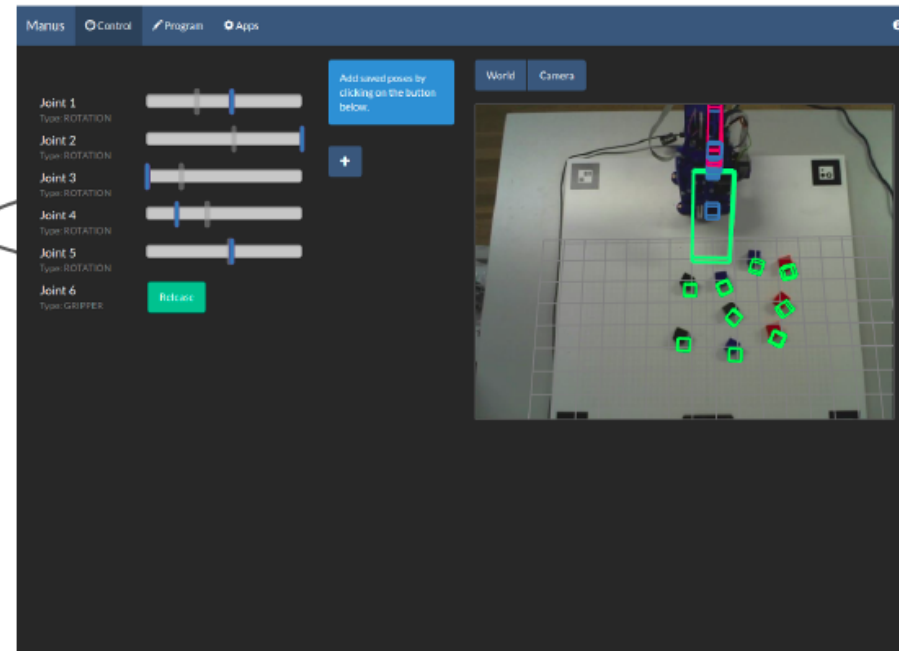
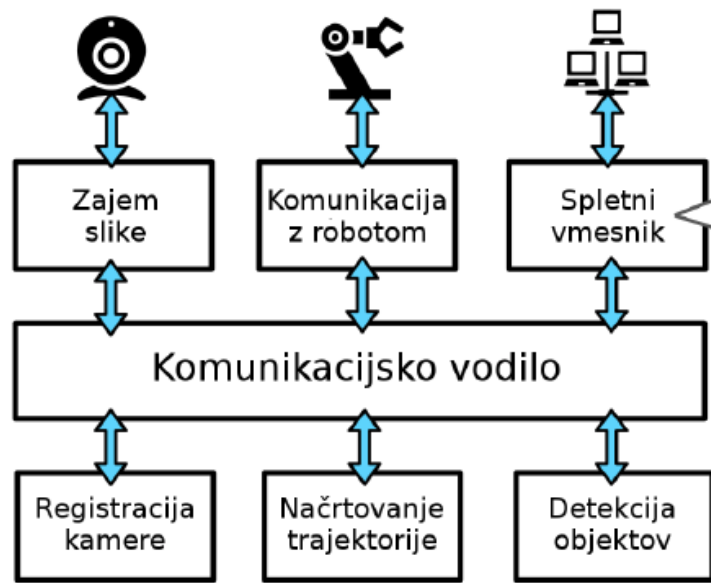


Lastnost	Vrednost
Višina	358 <i>mm</i>
Radij	310 <i>mm</i>
Ponovljivost	4 <i>mm</i>
Teža	842 <i>g</i>
Nosilnost	80 <i>g</i>
Napajanje	5,0 <i>V</i>
Tok	6000 <i>mA</i>

# Integration in ROS

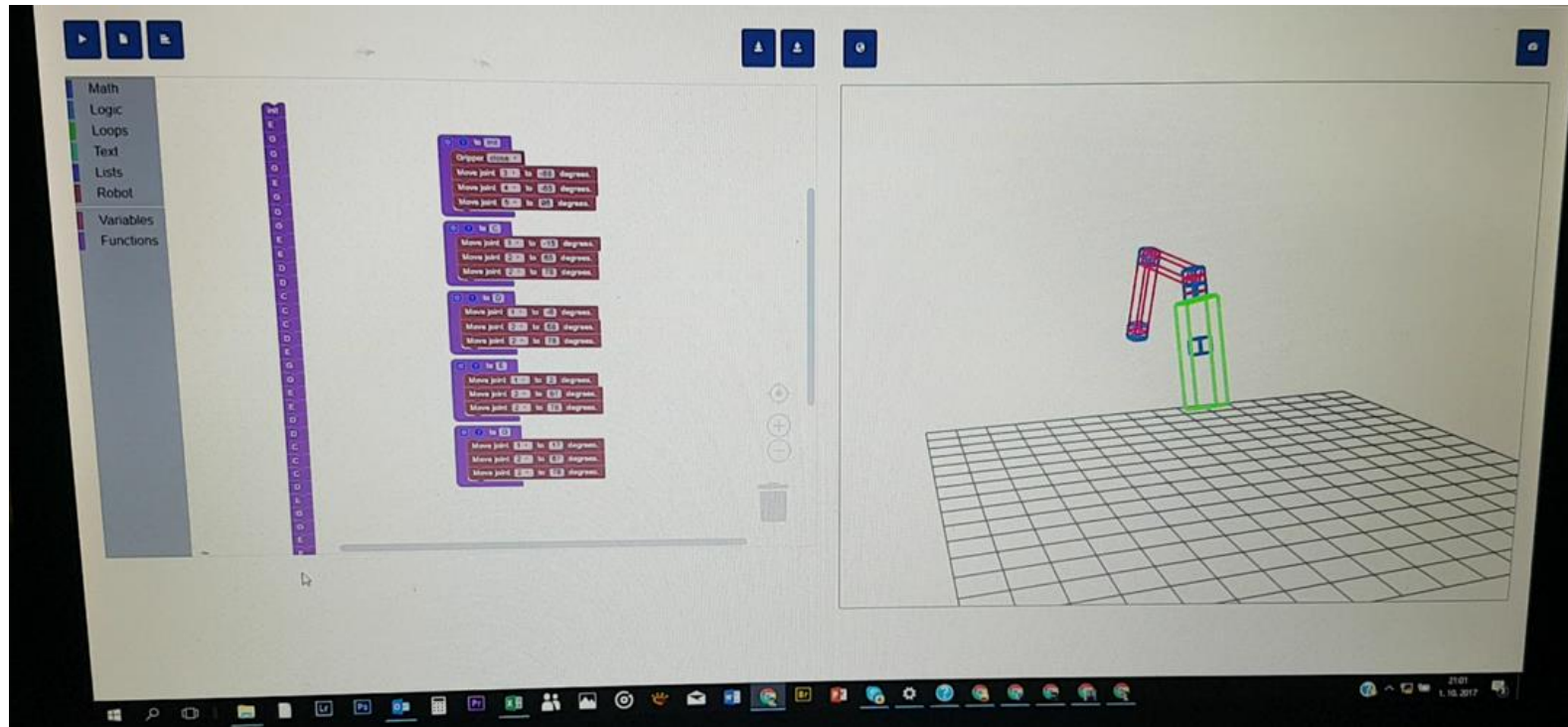


# Integration in Manus



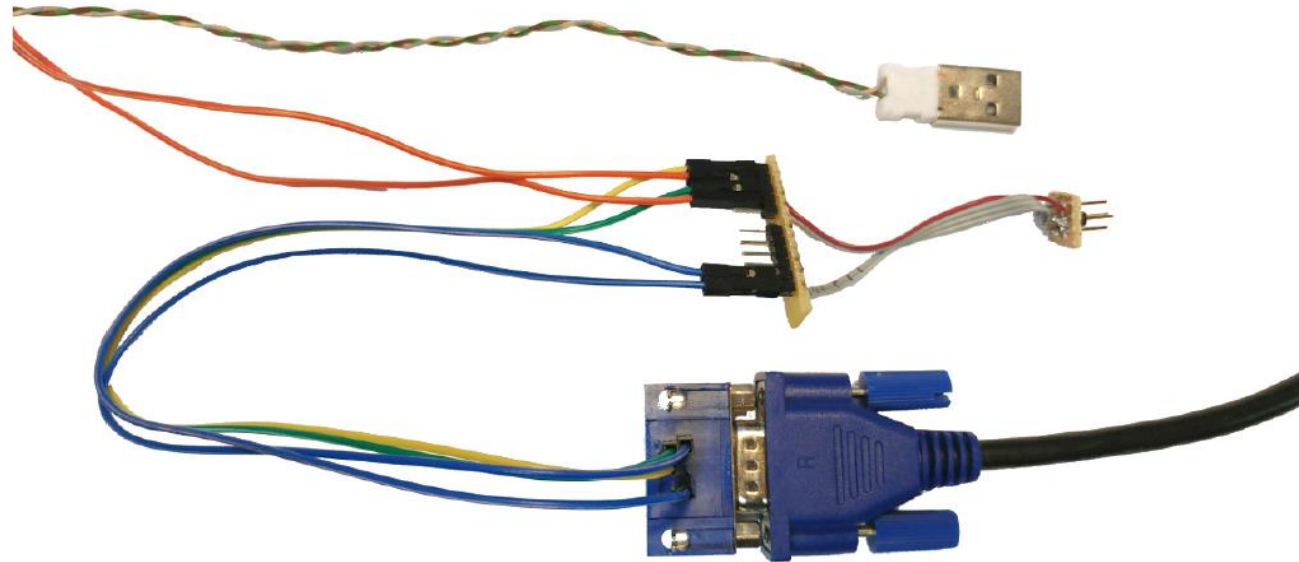
# Integration with programming languages

- Matlab
- Python
- Blockly

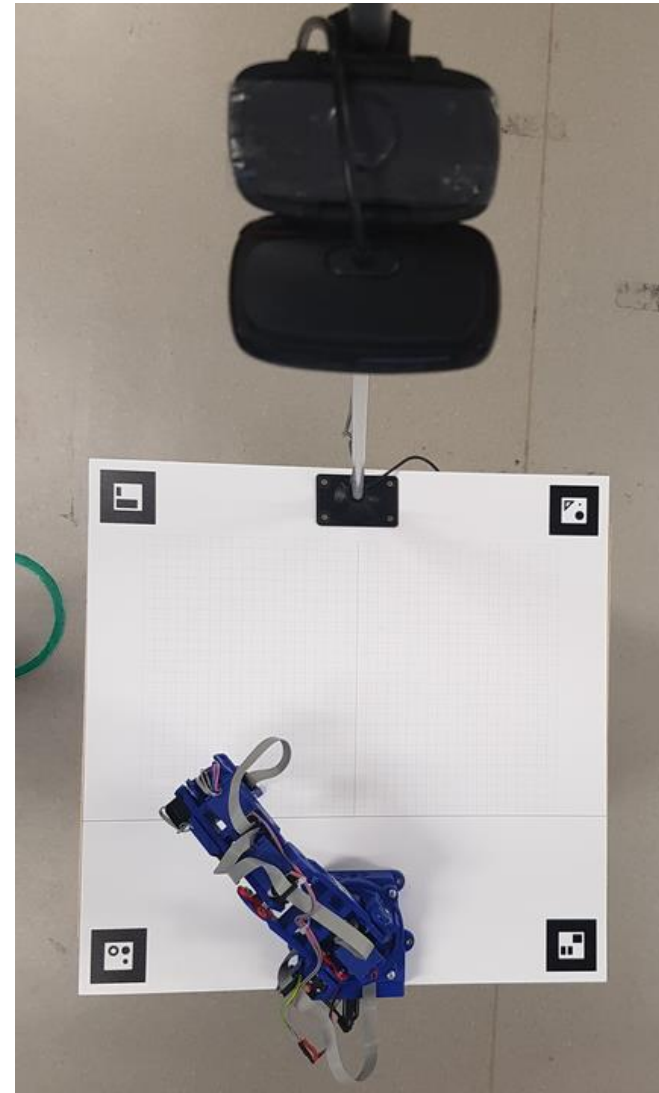
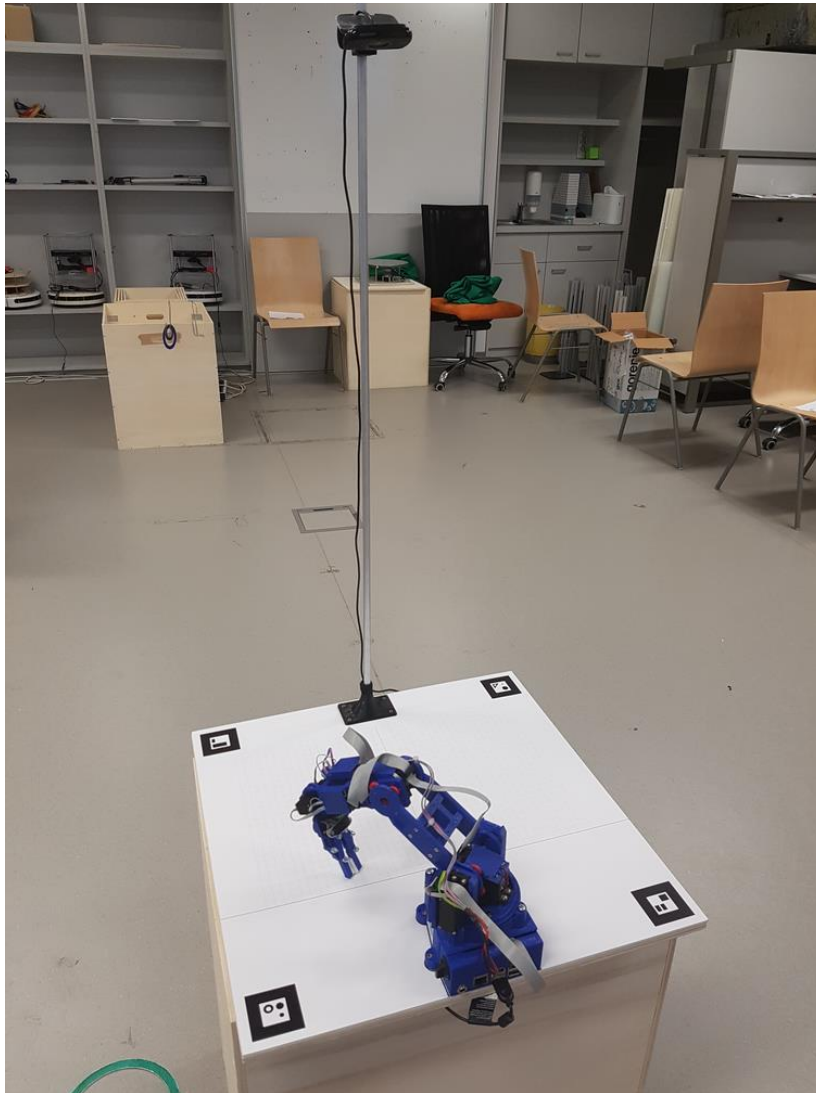


# Communication using VGA and USB cable

- VGA cable and I<sup>2</sup>C protocol
- USB port



# Registration with camera





# Augmented reality

## Camera view

USB Robot Manipulator (version: 0.10)

Joint 1  
Type: ROTATION

Joint 2  
Type: ROTATION

Joint 3  
Type: ROTATION

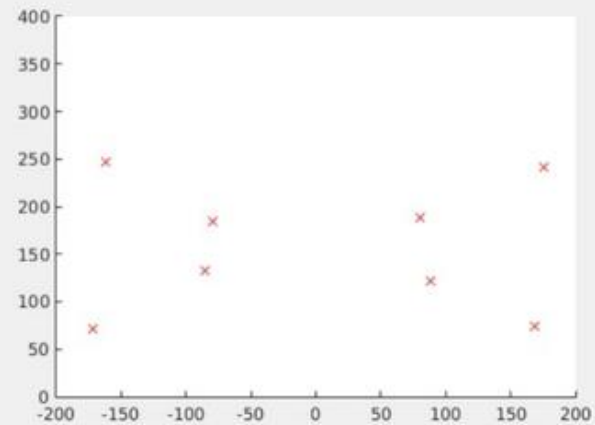
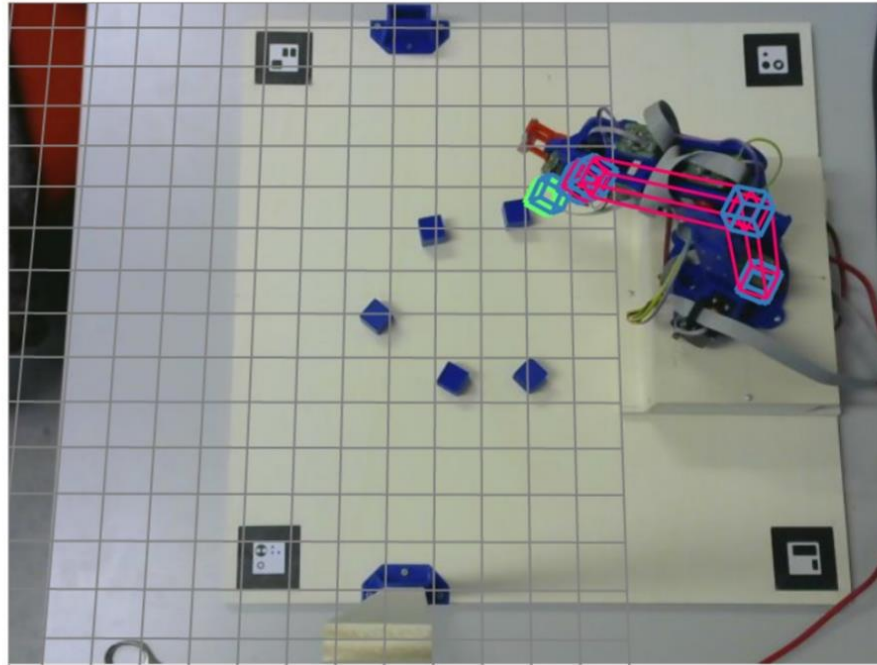
Joint 4  
Type: ROTATION

Joint 5  
Type: FIXED

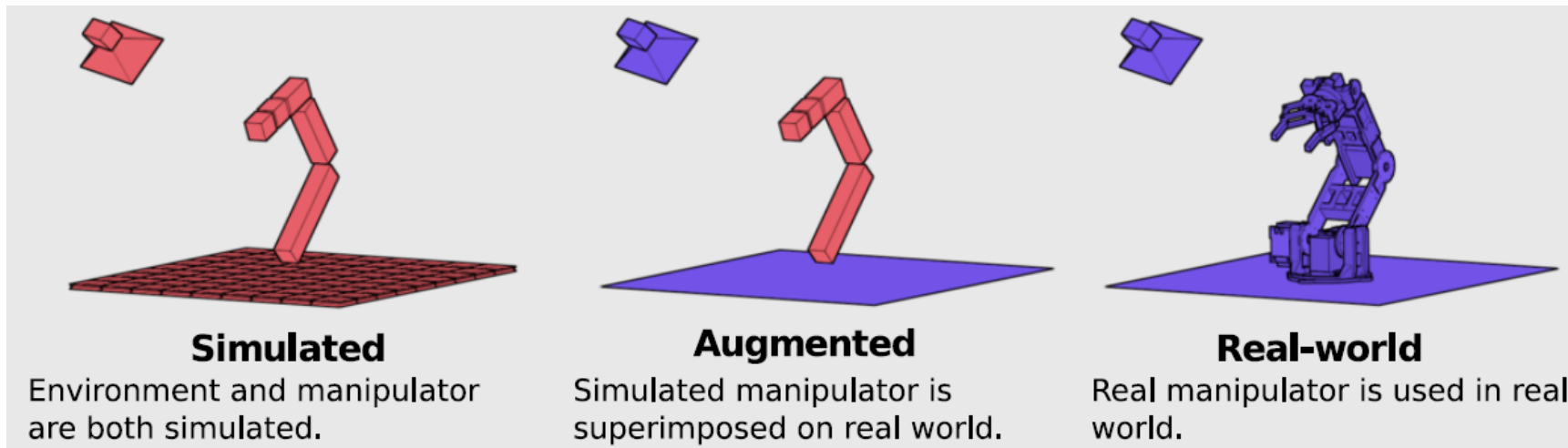
Joint 6  
Type: ROTATION

Joint 7  
Type: GRIPPER

Grip

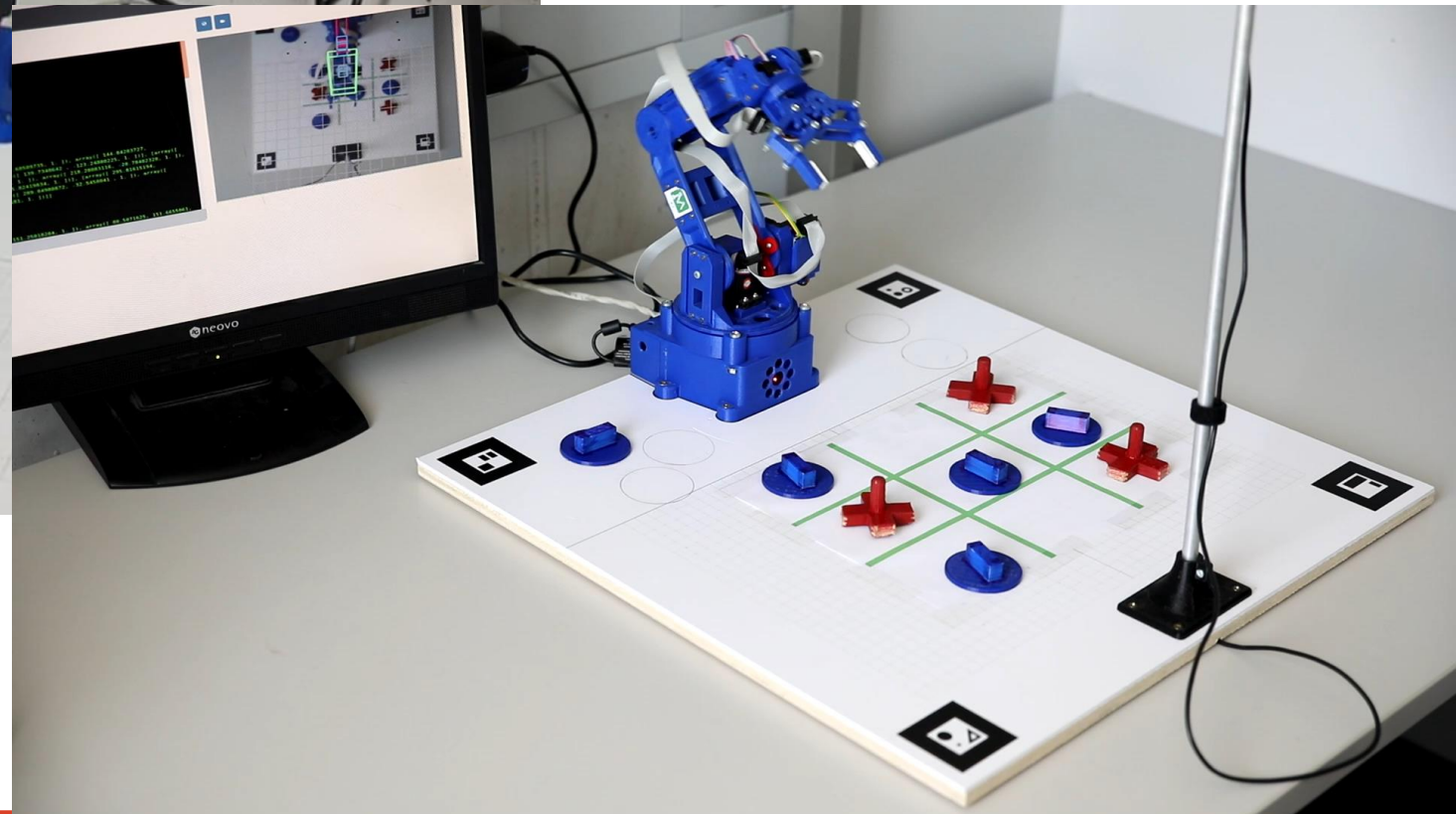
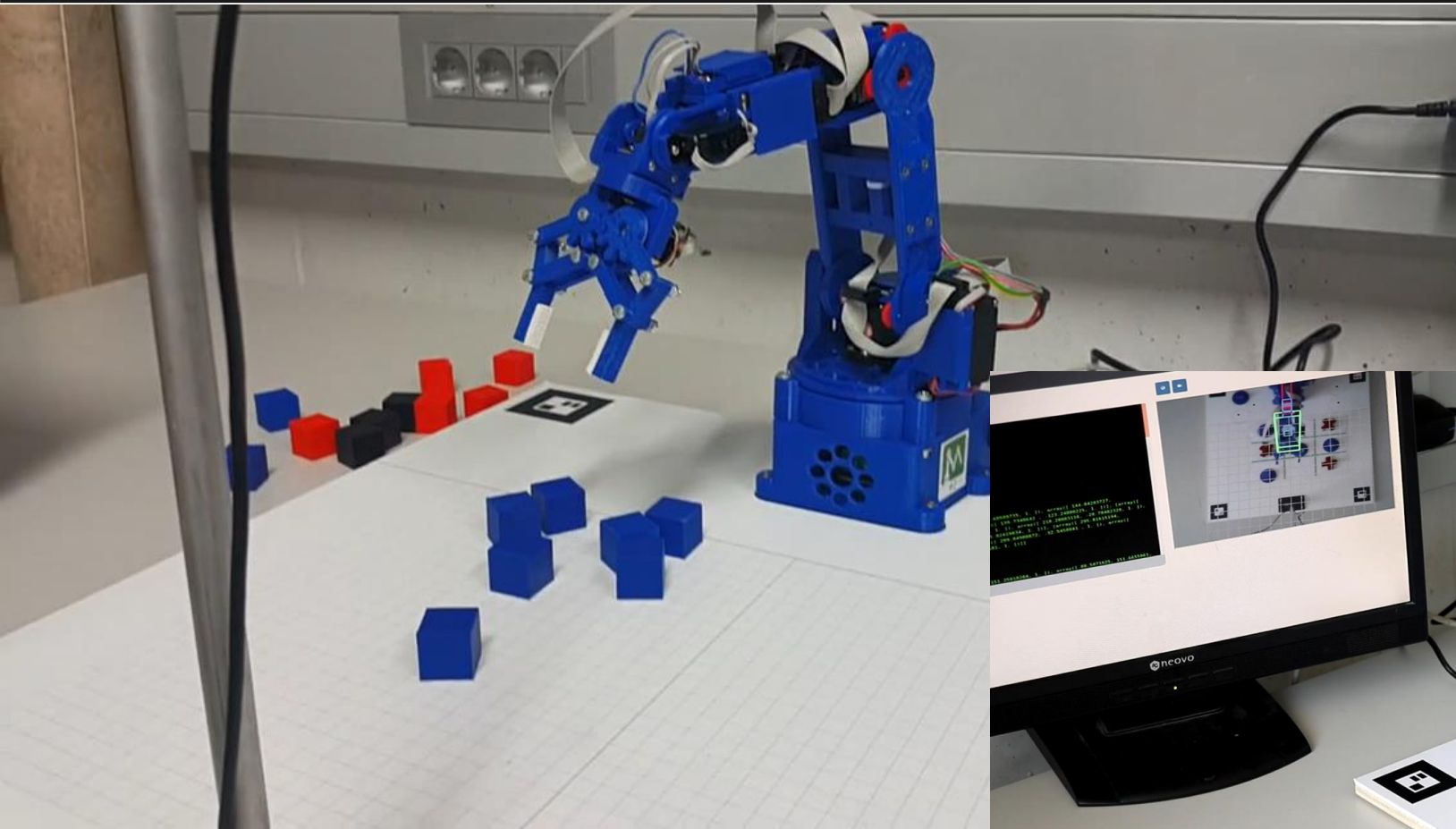


# Multi-level teaching approach



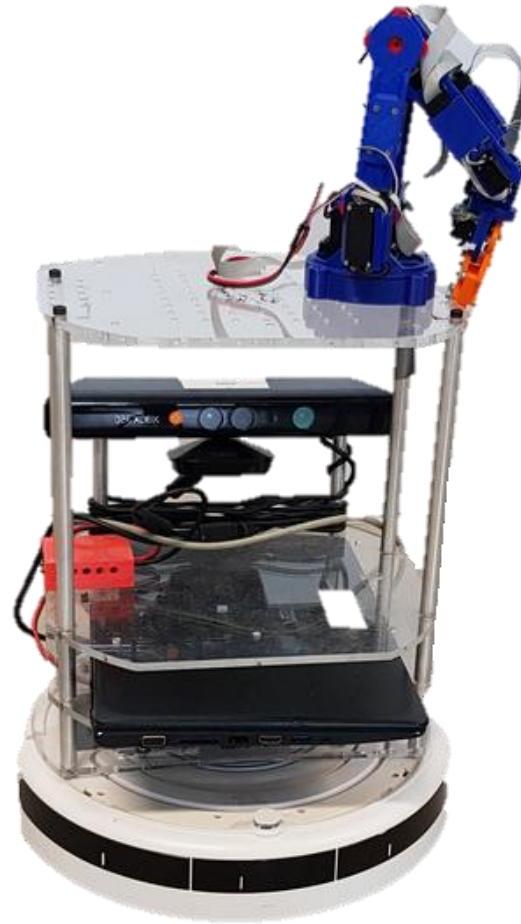
	perception	action	activity
1	simulated	none	Learning basic computer vision algorithms by processing stored images.
2	real	none	Learning more advanced computer vision algorithms by capturing and processing live images.
3	none	simulated	Learning the basics of robot manipulation in simulated environment.
4	none	real	Learning to operate the robot manipulator in the real world.
5	real	simulated	Detecting the objects in the scene and pointing at them with the virtual robot manipulator.
6	real	real	Detecting and grasping the objects in the scene with the physical robot manipulator.

# Video



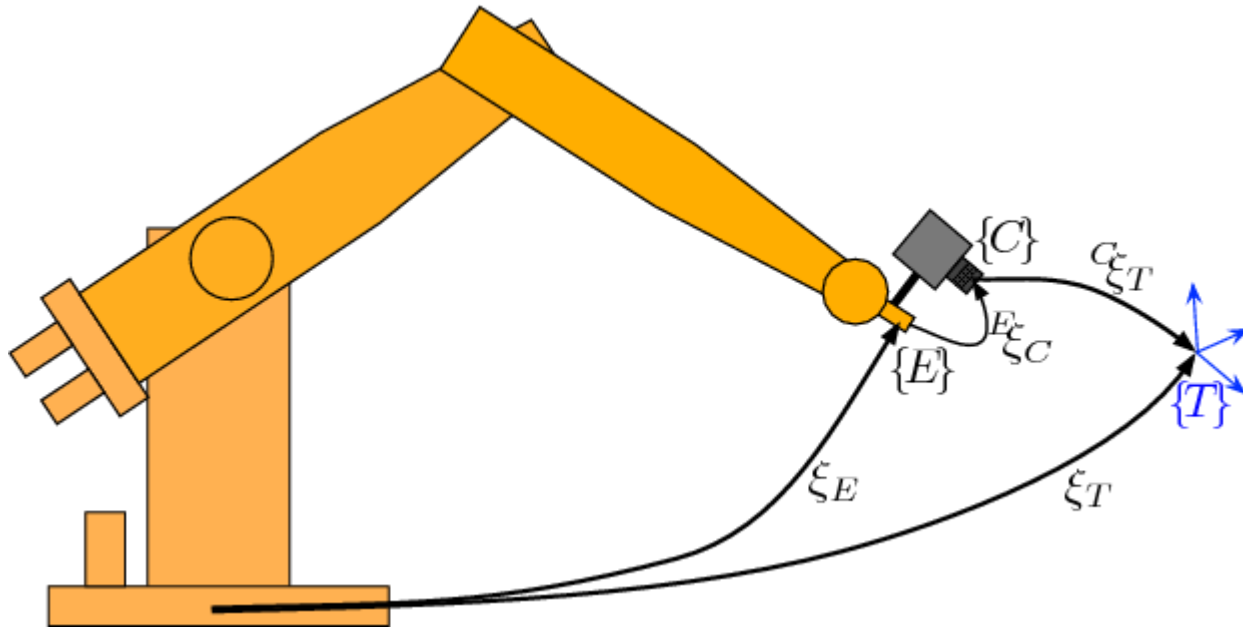
# Mobile manipulation

---

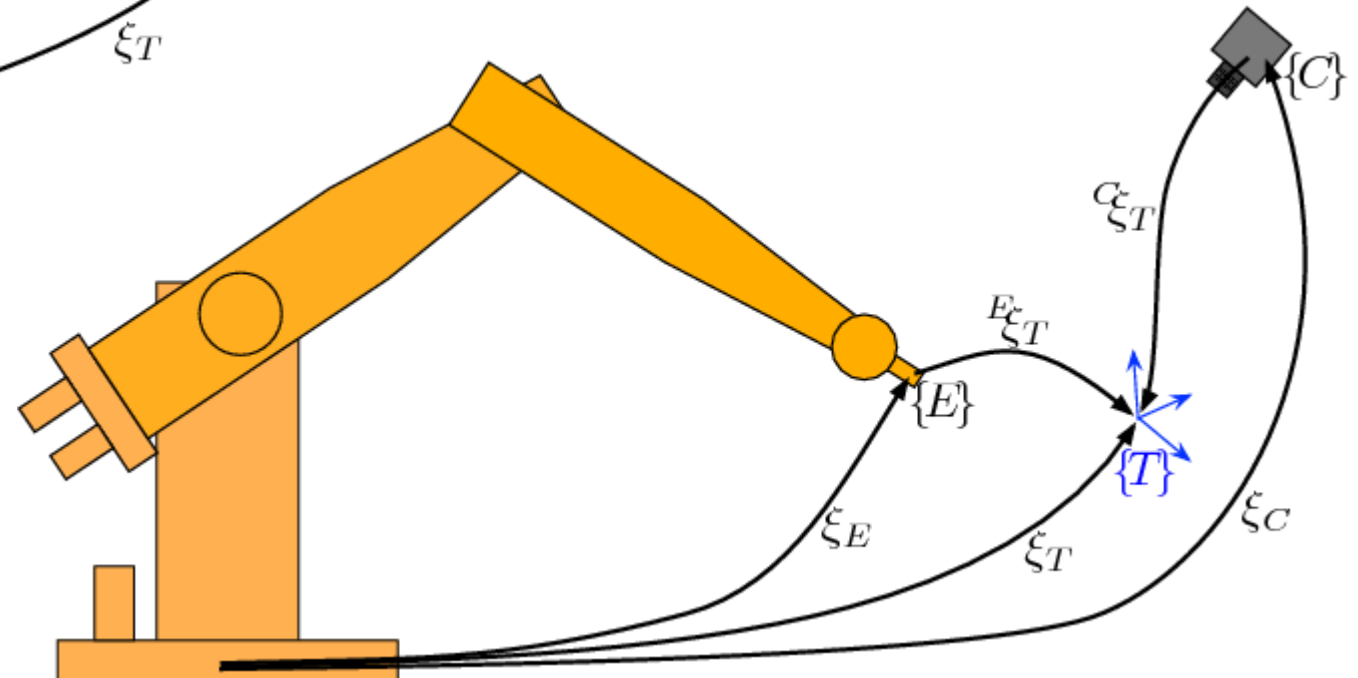


# Vision-based control

Moving the end effector to the desired pose determined by the pose of an object



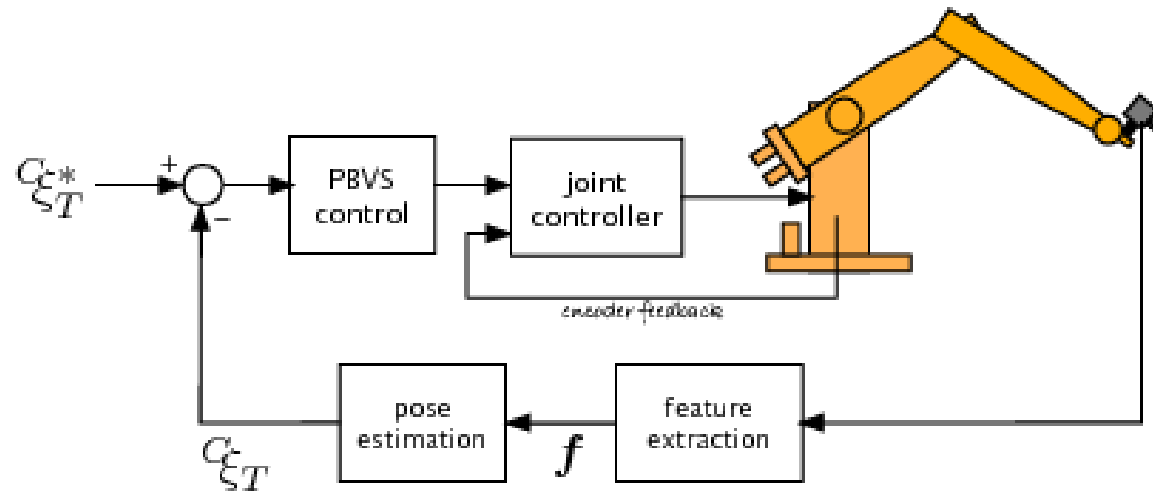
- Camera on the robot



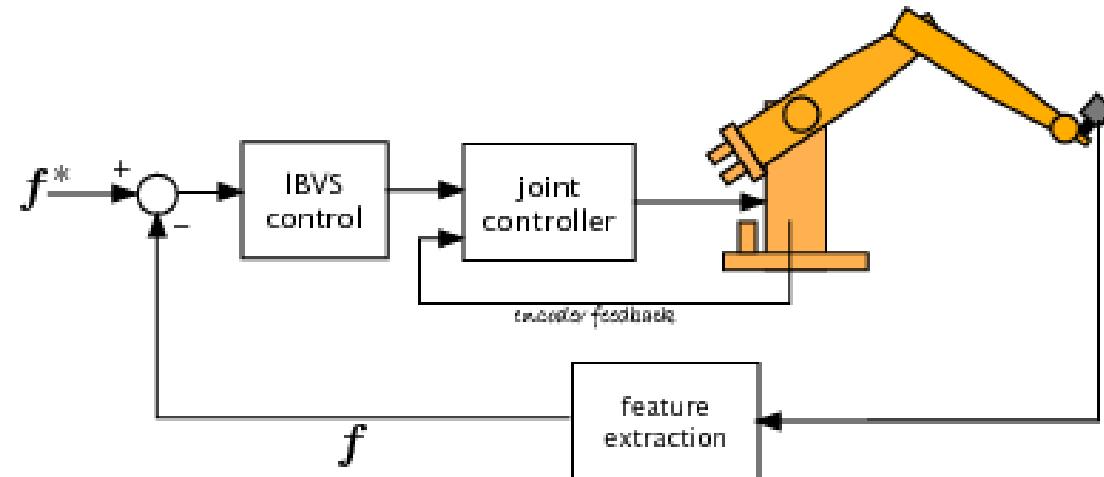
- Fixed camera

# Vision-based control

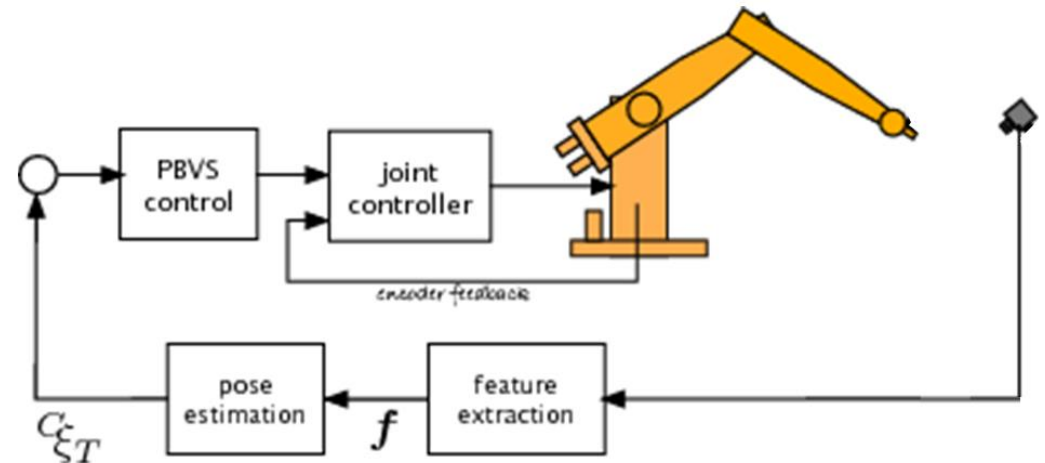
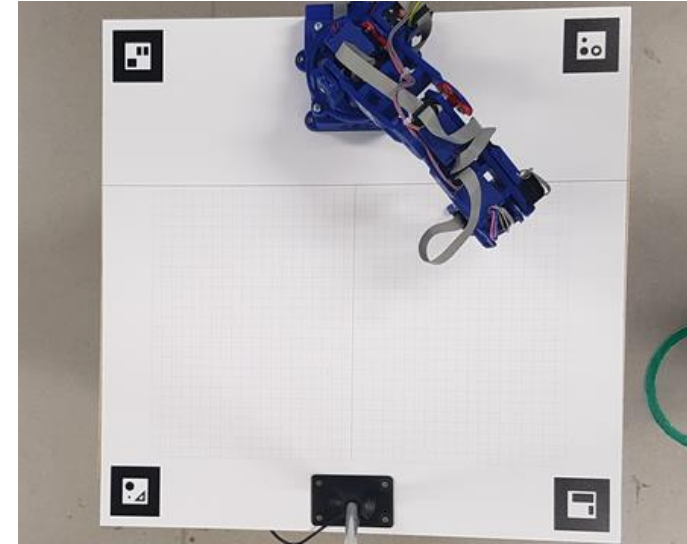
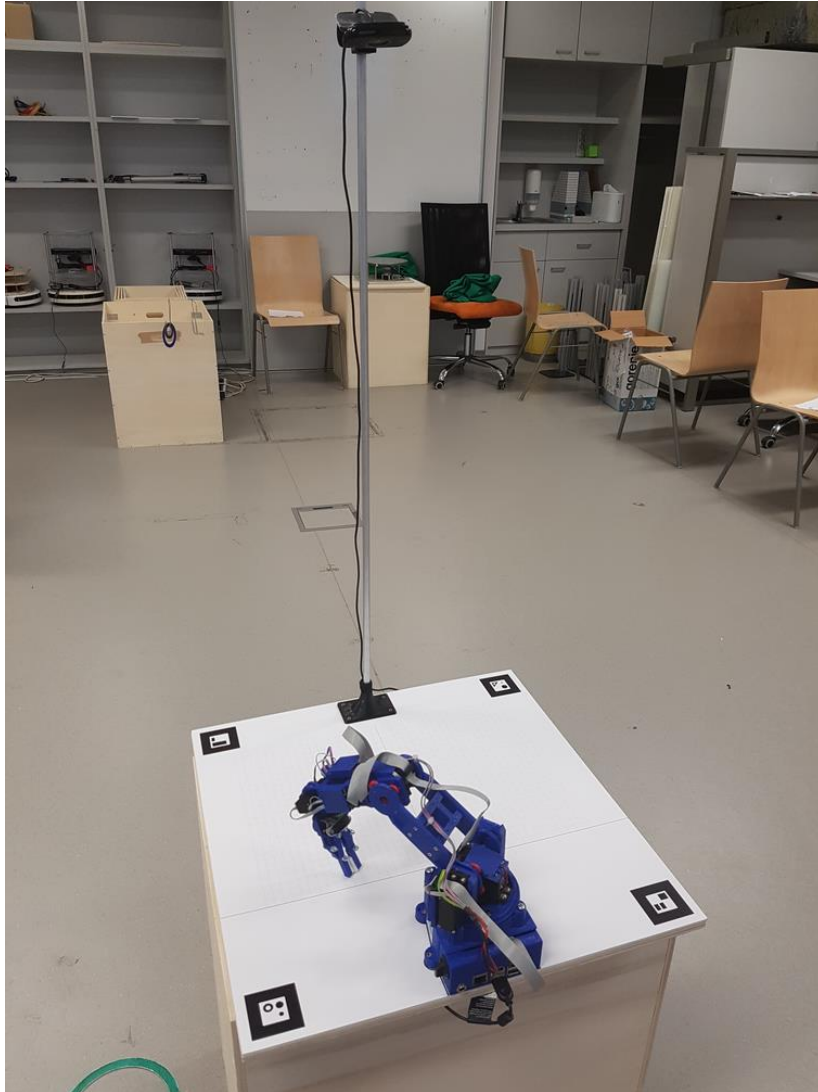
- Position-based servoing
  - Explicit control
  - In world coordinate frame



- Image-based servoing
  - Implicit control
  - In image coordinate frame



# Vision-based control



# Vision-based control

- Mobile manipulation
- Joint control of mobile robot and robot manipulator

